Appendix 5

DETAILED EMISSIONS CALCULATIONS

SHORT TERM EMISSIONS SUMMARY

		со	NOx	SO2	PM	PM10	VOC	Pb	HF	H2SO4	Hg
<u>ID</u>	Emission Unit(s)	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr	lb/hr
_											
C04	Combustion Sources	700	205	400	400	400	40.0	0.000	F 04	47.7	0.42
S01 S02	Unit 1 PC Boiler Unit 2 PC Boiler	782 782	365 365	462 462	198 198	198 198	18.8 18.8	0.092 0.092	5.04 5.04	17.7 17.7	0.13 0.13
S02	Unit 3 PC Boiler	782 782	365	462	198	198	18.8	0.092	5.04	17.7	0.13
S04 Rese		102	303	402	130	190	10.0	0.092	3.04	17.7	0.13
S05	Auxiliary Boiler (Distillate Oil-Fired)	14.7	36.7	0.57	18.4	18.4	1.10			0.022	
S06	Coal Handling Particulate Sources Railcar Unloading Station				1.46	0.51					
S07	Emergency Coal Pile				0.74	0.74					
S08	Emergency Pile Reclaim				0.28	0.28					
S09	Reserved										
S10	Stackout Transfer Point #2				2.71	0.95					
S11	Active Pile #1				1.48	1.48					
S12	Active Pile #2				1.48	1.48					
S13	Active Pile Reclaim				0.57	0.57					
S14	Reserved										
S15	Transfer Tower				0.57	0.57					
S16	Reserved				0.05	0.05					
S17 S18	Tripper Deck Inactive Pile				2.85 1.20	2.85 1.20					
310	mactive File				1.20	1.20					
	Ash Handling Particulate Sources										
S19	Reserved										
S20	Bottom Ash Transfer Point #1				0.012	4.3E-03					
S21	Reserved										
S22	Bottom Ash Bunker				0.012	4.3E-03					
S23	Bottom Ash Transfer Point #2				0.046	0.016					
S24	Reserved				0.046	0.040					
S25 S26	Bottom Ash Transfer Point #3 Fly Ash Silos				0.046 1.20	0.016 1.20					
S27	Fly Ash Mixing Station				0.57	0.57					
S28	Fly Ash Transfer Point #1				0.049	0.017					
S29	Reserved				0.0.0	0.011					
S30	Fly Ash Transfer Point #2				0.049	0.017					
S31	Reserved										
S32	On-Site Disposal Facility				1.36	0.33					
	Carban Handling Particulate Courses										
S33	Carbon Handling Particulate Sources Carbon Silo				0.60	0.60					
333	Carbon Silo			-	0.00	0.00			-		
	Lime Handling Particulate Sources										
S34	Reserved										
S35	Lime Railcar Unloading Station				3.62	3.62					
S36	Reserved										
S37	Lime Silo				1.20	1.20					
	Roadway Particulate Sources										
S38	Unpaved Roadway Travel				2.19	0.54					
S39	Paved Roadway Travel				0.63	0.12					
000	ravoa riodanaj riavo.				0.00	02					
	Emergency Diesel Engine Driven Engines										
S40-S43	Reserved										
S44	Emergency Diesel Engine Driven Generator	11.57	21.2	0.024	0.66	0.66	1.55			9.3E-04	
S45	Emergency Diesel Engine Driven Firewater Pump	2.57	2.97	4.9E-03	0.15	0.15	1.10			1.9E-04	
	Fuel Starage Tanks										
C46	Fuel Storage Tanks						0.038				
S46 S47	330,000 Gallon Distillate Oil Storage Tank 20,000 Gallon Diesel Fuel Storage Tank						4.0E-03				
S48	2,000 Gallon Diesel Fuel Storage Tank						3.9E-04				
S49	500 Gallon Diesel Fuel Storage Tank						1.9E-05				
S50	500 Gallon Unleaded Gasoline Storage Tank						8.5E-03				
	-										
Total Emi	ssions	2,376	1,156	1,387	639	633	60.1	0.28	15.1	53.2	0.39

White Pine Energy Associates, LLC Appendix 5 - Revised 08/25/2006

LONG TERM EMISSIONS SUMMARY

Contaction Source	<u>ID</u>	Emission Unit(s)	CO tons/yr	NOx tons/yr	SO2 tons/yr	PM tons/yr	PM10 tons/yr	VOC tons/yr	Pb tons/yr	HF tons/yr	H2SO4 tons/yr	Hg tons/yr
	C01		2 427	1 500	2.024	000	969	92.2	0.26	15.0	77 7	0.050
1,995 1,99												
Audilary Boller (Delimiter)			5,421	1,000	2,024	000	000	02.2	0.20	10.0	77.7	0.000
Section Sect			3.67	9.18	0.14	4.59	4.59	0.28			5.5E-03	
Section Sect		Coal Handling Particulate Sources										
	S06					1.53	0.53					
Solida												
Sees												
Still Active Pile #	S09											
Stock Pile #2												
State March Marc												
State Reserved												
Sife Transfer Tower						2.49	2.49					
Side Reserved						0.40	0.40					
Strict Fripper Dock						2.49	2.49					
Ash Handling Particulate Sources Ash Handling P						12	12					
## Ash Handling Particulate Sources S19												
Signar Seserved Signar	010	muotive i ne				0.27	0.20					
S20 Bottom Ash Transfer Point #1 "		Ash Handling Particulate Sources										
S21 Reserved												
S22 Bottom Ash Bunker						0.014	5.1E-03					
S24 Reserved Res							_					
S24 Reserved												
See Bottom Ash Transfer Point #3						0.014	5.1E-03					
See Fly Ash Silos						0.014	E 1E 02					
SZR Fly Ash Mixing Station 2.49 2.49												
S28												
Reserved S30 Fly Ash Transfer Point #2 0.071 0.025												
Sat												
Carbon Handling Particulate Sources Carbon Silo Carb	S30	Fly Ash Transfer Point #2				0.071	0.025					
Carbon Handling Particulate Sources Saster Silo Sast												
Lime Handling Particulate Sources Sa4 Reserved Sa5 Lime Railcar Unloading Station	S32	On-Site Disposal Facility				5.96	1.44					
Lime Handling Particulate Sources Sa4 Reserved Sa5 Lime Railcar Unloading Station		Carbon Handling Particulate Sources										
Signature Comparison Comp	633					2.62	2.62					
Reserved S35	000	Carbon Gilo				2.02	2.02					
Reserved S35		Lime Handling Particulate Sources										
Reserved Safe Company Safe	S34											
Roadway Particulate Sources S38	S35	Lime Railcar Unloading Station				16	16					
Roadway Particulate Sources S38 Unpaved Roadway Travel 1												
Sas	S37	Lime Silo				5.23	5.23					
Sas		Boodway Borticulata Sources										
Emergency Diesel Engine Driven Engines S40-S43 Reserved S44 Emergency Diesel Engine Driven Generator 2.89 5.29 6.1E-03 0.165 0.165 0.39 2.3E-04 S45 Emergency Diesel Engine Driven Firewater Pump 0.19 0.22 3.7E-04 0.011 0.011 0.083 1.4E-05 S47 20,000 Gallon Diesel Fuel Storage Tank 5.1E-04 S48 2,000 Gallon Diesel Fuel Storage Tank 1.1E-03 S49 500 Gallon Diesel Fuel Storage Tank 1.1E-03 S49 500 Gallon Diesel Fuel Storage Tank 1.9E-04 S49 500 Gallon Diesel Fuel Storage Tank	538					10	2 38					
Emergency Diesel Engine Driven Engines S40-S43 Reserved S44 Emergency Diesel Engine Driven Generator 2.89 5.29 6.1E-03 0.165 0.165 0.39 2.3E-04 S45 Emergency Diesel Engine Driven Firewater Pump 0.19 0.22 3.7E-04 0.011 0.011 0.083 1.4E-05 Storage Tanks S46 330,000 Gallon Distillate Oil Storage Tank 5.1E-04 S47 20,000 Gallon Diesel Fuel Storage Tank 5.1E-04 S48 2,000 Gallon Diesel Fuel Storage Tank 1.1E-03 S49 500 Gallon Diesel Fuel Storage Tank 1.9E-04 S50 500 Gallon Unleaded Gasoline Storage Tank 0.27												
\$40-\$43 Reserved \$44 Emergency Diesel Engine Driven Generator 2.89 5.29 6.1E-03 0.165 0.165 0.39 2.3E-04 \$45 Emergency Diesel Engine Driven Firewater Pump 0.19 0.22 3.7E-04 0.011 0.011 0.083 1.4E-05 Storage Tanks \$46 330,000 Gallon Diestllate Oil Storage Tank 0.063 \$47 20,000 Gallon Diesel Fuel Storage Tank 5.1E-04 \$48 2,000 Gallon Diesel Fuel Storage Tank 5.1E-04 \$49 500 Gallon Diesel Fuel Storage Tank		,,,,										
S44 Emergency Diesel Engine Driven Generator 2.89 5.29 6.1E-03 0.165 0.39 2.3E-04 S45 Emergency Diesel Engine Driven Firewater Pump 0.19 0.22 3.7E-04 0.011 0.011 0.083 1.4E-05 Storage Tanks S46 330,000 Gallon Distillate Oil Storage Tank <		Emergency Diesel Engine Driven Engines										
S45 Emergency Diesel Engine Driven Firewater Pump 0.19 0.22 3.7E-04 0.011 0.011 0.083 1.4E-05 Storage Tanks S46 330,000 Gallon Distrillate Oil Storage Tank												
Storage Tanks S46 330,000 Gallon Distillate Oil Storage Tank												
S46 330,000 Gallon Distillate Oil Storage Tank 0.063	S45	Emergency Diesel Engine Driven Firewater Pump	0.19	0.22	3.7E-04	0.011	0.011	0.083			1.4E-05	
S46 330,000 Gallon Distillate Oil Storage Tank 0.063		Storage Tanks										
S47 20,000 Gallon Diesel Fuel Storage Tank 5.1E-04 S48 2,000 Gallon Diesel Fuel Storage Tank	S46							0.063				
\$48 2,000 Gallon Diesel Fuel Storage Tank 1.1E-03 \$49 500 Gallon Diesel Fuel Storage Tank												
S49 500 Gallon Diesel Fuel Storage Tank 1.9E-04 S50 500 Gallon Unleaded Gasoline Storage Tank												
S50 500 Gallon Unleaded Gasoline Storage Tank 0.27												
Total Emissions 10,287 4,812 6,071 2,704 2,687 248 0.79 46.0 233 0.15	S50							0.27				
Total Emissions 10,287 4,812 6,071 2,704 2,687 248 0.79 46.0 233 0.15	- :		40				0.5			46 -	05-	
	Total Emi	ssions	10,287	4,812	6,071	2,704	2,687	248	0.79	46.0	233	0.15

White Pine Energy Associates, LLC Appendix 5 - Revised 08/25/2006

I. PC BOILERS S01, S02, and S03				S01, S02, and	4 603		
	-	Load C	ondition	301, 302, and		Averaging Per	iod
	Min.	50%	75%	100%	3-hr	24-hr	Annual
Megawatts (Gross)	147	291	432	576	576	576	576
Megawatts (Net) Heat Input (MMBtu/hr, HHV)	133 1,468	265 2,763	398 3,986	530 5,216	530 5,216	530 5,216	530 5,216
• • • • • •							
Coal HHV (Btu/lb)	8,200	8,200	8,200	8,200	8,200	8,200	8,200
Design Sulfur (%) Max Sulfur (%)	0.46% 0.66%	0.46% 0.66%	0.46% 0.66%	0.46% 0.66%	0.46% 0.66%	0.46% 0.66%	0.46% 0.66%
Coal flow (lb/hr)	179,069	336,945	486,049	636,158	636,158	636,158	636,158
Coal Flow (tons/hr)	90	168	243	318	318	318	318
Stack Exit Temperature (deg F)	165	165	165	165	165	165	165
Stack Exit Temperature (deg F) Stack Exit Flow (lb/hr)	165 1,757,432	165 3,209,524	4,348,988	165 5,692,172	165 5,692,172	165 5,692,172	165 5,692,172
Stack Exit Flow (acfm)	468,211	853,866	1,153,416	1,509,649	1,509,649	1,509,649	1,509,649
Stack Diameter (ft)	22.2	22.2	22.2	22.2	22.2	22.2	22.2
Stack Velocity (ft/sec)	20	37	50	65	65	65	65
СО							
lb/MMBtu	0.15	0.15	0.15	0.15		0.15	0.15
lb/hr	220.20	414.45	597.90	782.40		782.40	782.40
tpy							3,426.9
NOx							
lb/MMBtu before SCR	0.30	0.30	0.30	0.30		0.30	0.30
% Control lb/MMBtu	77% 0.07	77% 0.07	77% 0.07	77% 0.07		77% 0.07	77% 0.07
lb/hr	102.76	193.41	279.02	365.12	 	365.12	365.12
tpy							1,599.2
000							
SO2 Ib/MMBtu before scrubber *	1.61	1.61	1.61	1.61		1.61	1.61
% Control	94%	94%	94%	94%		94%	94%
lb/MMBtu after scrubber *	0.09	0.09	0.09	0.09		0.09	0.09
lb/hr after scrubber	130.0	245.0	353.0	462.0		462.0	462.0
tpy after scrubber							2,023.6
PM/PM10 - total, controlled							
lb/MMBtu	0.038	0.038	0.038	0.038	0.038		0.038
lb/hr	55.78	104.99	151.47	198.21	198.21		198.21
tpy							868.2
PM/PM10 - filterable, controlled							
lb/MMBtu	0.015	0.015	0.015	0.015	0.015		0.015
lb/hr	22.02	41.45	59.79	78.24	78.24		78.24
tpy							342.7
VOC							
lb/MMBtu	3.6E-03	3.6E-03	3.6E-03	3.6E-03	3.6E-03		3.6E-03
lb/hr	5.28	9.95	14.35	18.78	18.78		18.78
tpy							82.2
Lead							
ppm, uncontrolled	9.48	9.48	9.48	9.48	15		9.48
% Control	99%	99%	99%	99%	99%		99%
lb/MMBtu	1.2E-05	1.2E-05	1.2E-05	1.2E-05	1.8E-05		1.2E-05
lb/hr tpy	0.017	0.032	0.046	0.060	0.092		0.060 0.264
фу							0.204
Fluoride (as HF)							
ppm, uncontrolled	105	105	105	105	151		105
% Control lb/MMBtu	95% 6.7E-04	95% 6.7E-04	95% 6.7E-04	95% 6.7E-04	95% 9.7E-04		95% 6.7E-04
lb/hr	0.98	1.85	2.67	3.50	5.04		3.50
tpy							15.32
110004							
H2SO4 Ib/MMBtu before scrubber	0.062	0.062	0.062	0.062	0.043		0.062
% Control	92%	92%	92%	92%	92%		92%
lb/MMBtu *	4.9E-03	3.4E-03	3.4E-03	3.4E-03	3.4E-03		3.4E-03
lb/hr	7.23	9.39	13.55	17.73	17.73		17.73
tpy							77.7
Hg							
lb/MW-hr	2.0E-05	2.0E-05	2.0E-05	2.0E-05	. 		2.0E-05
lb/MMBtu					2.5E-05		
lb/hr tpy	0.003	0.006	0.009	0.012	0.130 		0.012 0.050
47							0.000
NH3 Slip							
ppm	5	5	5	5	10		5
lb/hr tov	4.50 	8.00	10.50 	14.60	41.00 		14.60 64.0
tpy		-	-				U4.U
HCI					_		
ppm, uncontrolled	215	215	215	215	329		215
% Control lb/MMBtu	95% 1.3E-03	95% 1.3E-03	95% 1.3E-03	95% 1.3E-03	95% 2.1E-03		95% 1.3E-03
lb/hr	1.979	3.724	5.373	7.031	10.759		7.031
tpy							30.8

^{*} Values based on potential to emit versus design coal.

II. AUXILIARY BOILER

S04 Reserved

S05 Auxiliary Boiler

Heat Input (MMBtu/hr) Fuel Heating Value (Btu/lb) Fuel Density (lb/gal) Fuel Flow (lb/hr) Annual Operating Hours Annual Fuel (gal) Fuel Sulfur (ppm)	367 19,200 7.23 19,115 500 1,321,894
Stack Temperature (deg F) Stack Height (ft) Stack Diameter (ft) Stack Flow (acfm)	670 225 7.24 146,800
CO Ib/MMBtu Ib/hr ton/year	0.04 14.7 3.67
NOx Ib/MMBtu Ib/hr ton/year	0.1 36.7 9.18
SO2 Ib/MMBtu Ib/hr ton/year	1.6E-03 0.57 0.14
PM/PM10 - total lb/MMBtu lb/hr ton/year	0.05 18.4 4.59
PM/PM10 - filterable lb/MMBtu lb/hr ton/year	0.01 3.67 0.92
VOC Ib/MMBtu Ib/hr ton/year	0.003 1.10 0.28
H2SO4 Ib/MMBtu Ib/hr ton/year	6.0E-05 0.022 5.5E-03

Notes: Emission rates are based on discussions with vendors.

SO2 emission rate based on fuel sulfur content.

H2SO4 emission rate based on fuel sulfur content and 2.5% oxidation rate.

III. COAL HANDLING PARTICULATE EMISSIONS

S06 Railcar Unloading Station

Railcars will be brought into a partially enclosed railcar unloading structure. The railcars will be connected with a rotary coupling so they can be tipped to dump the coal. The coal will be dumped into an underground hopper. From the underground hopper the coal will be transferred to a short conveyor and then transferred to stackout conveyor #1. A dust suppression spray will be used to control dust emissions from the railcar unloader. The sprayed water will also reduce emissions throughout the downstream conveying process. The hopper, short conveyor and two transfer points are located in an enclosed area under the Railcar Unloading Station.

Coal Throughput Design Data

Maximum coal transfer rate: 4,000 tons/hr 8,359,116 tons/yr

Assumes full load operation for 8,760 hours per year

S06 Emissions from Railcar Unloading

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum expected throughput per year.

Emission factor : $\left(\frac{\text{lb emissions}}{\text{ton coal}} \right) = k * 0.0032 * \frac{\left(\frac{\text{U}}{5} \right)^{1.3}}{\left(\frac{\text{M}}{2} \right)^{1.4}}$

where: k = particulate multiplier = 1 for PM k = particulate multiplier = 0.35 for PM10

U = mean wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data
M = material moisture content in % = 6.9 average moisture content of coal

PM Emission factor: 1.36E-03 lb/ton PM10 Emission factor: 4.74E-04 lb/ton

Control efficiency: 87.5% for water sprays plus partial enclosure

PM = 0.68 lb/hr PM = 0.71 tons/yr PM10 = 0.24 lb/hr PM10 = 0.25 tons/yr

S06 Emissions from hopper drop to short conveyor and from short conveyor drop to stackout conveyor #1

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum expected throughput per year. Two transfer points are calculated.

Emission factor : $\left(\frac{\text{lb emissions}}{\text{ton coal}} \right) = k * 0.0032 * \frac{\left(\frac{U}{5} \right)^{1.3}}{\left(\frac{M}{2} \right)^{1.4}}$

where: k = particulate multiplier = 1 for PM
k = particulate multiplier = 0.35 for PM10
U = mean wind speed (mph) = 1.3 conservative estimate for wind speed in enclosure
M = material moisture content (%) = 6.9 average moisture content of coal

PM Emission factor: 9.81E-05 lb/ton PM10 Emission factor: 3.43E-05 lb/ton

PM = 0.78 lb/hr includes two transfer points PM = 0.82 tons/yi includes two transfer points PM10 =0.27 lb/hr includes two transfer points PM10 =0.29 tons/yi includes two transfer points

Combined Emissions at Railcar Unloading Station

PM = 1.46 lb/hr PM = 1.53 tons/yr PM10 = 0.51 lb/hr PM10 = 0.53 tons/yr

S07 <u>Emergency Coal Pile</u>

The Emergency Coal Pile and reclaim will be in use during maintenance or repair of the Active Pile Reclaim. During those times, the Emergency Coal Pile will have an approximate exposed surface area of 0.70 acres assuming a cone shaped pile with an approximate base diameter of 173 feet and height of 65 feet. Fugitive dust emissions will be controlled by dust suppression water sprays.

Coal Pile Design Data

Area of coal pile: 0.70 acres

Emissions

Emissions are calculated using the EPA AP-42, Section 11.9.1 emission factor calculation for an active storage pile (wind erosion and maintenance bulldozing). PM and PM10 emissions are computed as TSP <= 30 um. Use of TSP <= 30 um is a conservative estimate for PM10.

Emission factor : $\left(\frac{lb}{acre - hr}\right) = 0.72u$

where: u = average wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data

Emission factor: 7.06 lb/acre-hr

Control efficiency: 85% for fogging water sprays

PM = 0.74 lb/hr PM = 3.25 tons/yr PM10 = 0.74 lb/hr PM10 = 3.25 tons/yr

S08 <u>Emergency Pile Relclaim</u>

Coal will be transferred from the Emergency Coal Pile to the emergency conveyor via a drop operation under the Emergency Coal Pile. The emergency conveyor will transport the coal to the Transfer Tower. The drop onto the emergency conveyor will take place in an enclosed area under the Emergency Coal Pile. The Emergency Pile Reclaim will be enclosed and all emissions will exhaust through a fabric filter.

Filter Design Data

Stack Diameter 1.0 feet Stack Flow 3,320 dscfm

Emissions from Emergency Coal Pile drop to emergency conveyor

The fabric filter will use bags with a maximum emission rate of 0.01 gr/dscf. The estimated stack flow rate and 0.01 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.01 grains/dscf

PM = 0.28 lb/hr PM = 1.25 tons/yr PM10 = 0.28 lb/hr PM10 = 1.25 tons/yr

S09 Reserved

S10 Stackout Transfer Point #2 (stackout conveyor #2 to Active Pile #1 or #2)

From stackout conveyor #1, coal is transferred onto stackout conveyor #2 by drop operation in the Transfer Tower, mentioned below. Coal will be transferred from stackout conveyor #2 to Active Pile #1 or Active Pile #2 by drop operation at the Stackout Transfer Point #2 via stackout tube.

Coal Throughput Design Data

Maximum coal transfer rate: 4,000 tons/hr 8,359,116 tons/yr Assumes full load operation for 8,760 hours per year

Emissions

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum expected throughput per year.

Emission factor :
$$\left(\frac{\text{lb emissions}}{\text{ton coal}} \right) = k * 0.0032 * \frac{\left(\frac{U}{5} \right)^{1.3}}{\left(\frac{M}{2} \right)^{1.4}}$$

where: k = particulate multiplier = 1 for PM k = particulate multiplier = 0.35 for PM10

M = material moisture content (%)

= 9.8 average of 7 years of Ely SCRAM data
M = material moisture content (%)

= 6.9 average moisture content of coal

 PM Emission factor:
 1.36E-03
 lb/ton

 PM10 Emission factor:
 4.74E-04
 lb/ton

Control efficiency: 50% for telescopic chute

 $\begin{array}{llll} PM = & 2.71 & lb/hr \\ PM = & 2.83 & tons/yr \\ PM10 = & 0.95 & lb/hr \\ PM10 = & 0.99 & tons/yr \\ \end{array}$

S11 Active Pile #1

Active Pile #1 will have an approximate exposed surface area of 1.4 acres assuming a cone shaped pile with an approximate base diameter of 244 feet and height of 92 feet. Fugitive dust emissions will be controlled by dust suppression water sprays.

Coal Pile Design Data

Area of coal pile: 1.4 acres

Emissions

Emissions are calculated using the EPA AP-42, Section 11.9.1 emission factor calculation for an active storage pile (wind erosion and maintenance bulldozing). PM and PM10 emissions are computed as TSP <= 30 um. Use of TSP <= 30 um is a conservative estimate for PM10.

Emission factor : $\left(\frac{lb}{acre - hr} \right) = 0.72u$

where: u = average wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data

Emission factor: 7.06 lb/acre-hr
Control efficiency: 85% for fogging water sprays

PM = 1.48 lb/hr PM = 6.49 tons/yr PM10 = 1.48 lb/hr PM10 = 6.49 tons/yr

S12 Active Pile #2

Active Pile #2 will have an approximate exposed surface area of 1.4 acres assuming a cone shaped pile with an approximate base diameter of 244 feet and height of 92 feet. Fugitive dust emissions will be controlled by dust suppression water sprays.

Coal Pile Design Data

Area of coal pile: 1.4 acres

Emissions

Emissions are calculated using the EPA AP-42, Section 11.9.1 emission factor calculation for an active storage pile (wind erosion and maintenance bulldozing). PM and PM10 emissions are computed as TSP <= 30 um. Use of TSP <= 30 um is a conservative estimate for PM10.

Emission factor: $\left(\frac{lb}{acre - hr}\right) = 0.72u$

where: u = average wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data

Emission factor: 7.06 lb/acre-hr

Control efficiency: 85% for fogging water sprays

PM = 1.48 lb/hr PM = 6.49 tons/yr PM10 = 1.48 lb/hr PM10 = 6.49 tons/yr

S13 Active Pile Relclaim

Coal will be transferred from the Active Piles to the active pile conveyor via a drop operation under the Active Piles. From the active pile conveyor, the coal will be dropped onto reclaim conveyor #1. The drop onto the active pile conveyor and the drop onto reclaim conveyor #1 will take place in an enclosed area under the Active Piles. The Active Pile Reclaim will be enclosed and all emissions will exhaust through a fabric filter.

Filter Design Data

Stack Diameter 1.5 feet Stack Flow 6.640 dscfm

Emissions from Active Piles drop to active pile conveyor and active pile conveyor to reclaim conveyor #1

The fabric filter will use bags with a maximum emission rate of 0.01 gr/dscf. The estimated stack flow rate and 0.01 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.01 grains/dscf

PM = 0.57 lb/hr PM = 2.49 tons/yr PM10 = 0.57 lb/hr PM10 = 2.49 tons/yr

S14 Reserved

S15 <u>Transfer Tower</u>

The Transfer Tower will receive coal from stackout conveyor #1 (from Railcar Unloading), reclaim conveyor #1 (from Active Piles), and emergency conveyor (from Emergency Coal Pile) for transfer onto stackout conveyor #2 (for transfer to the Active Piles) and reclaim conveyor #2 (for transfer to the boilers). The Transfer Tower may also contain a crusher for crushing any large pieces of coal. The Transfer Tower will be enclosed and all emissions will exhaust through a fabric filter.

Filter Design Data

Stack Diameter 1.5 feet Stack Flow 6,640 dscfm

Emissions from Transfers and Crusher

The fabric filter will use bags with a maximum emission rate of 0.01 gr/dscf. The estimated stack flow rate and 0.01 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.01 grains/dscf

PM = 0.57 lb/hr PM = 2.49 tons/yr PM10 = 0.57 lb/hr PM10 = 2.49 tons/yr

S16 Reserved

S17 Tripper Deck

The tripper deck conveyor will receive coal from reclaim conveyor #2 and transport it to the storage silos. The tripper deck conveyor, silos and two transfer points will be enclosed and the enclosure will exhaust through a fabric filter.

Filter Design Data

Stack Diameter 3.0 feet Stack Flow 33,200 dscfm

Emissions from reclaim conveyor #2 drop to tripper deck conveyor and tripper deck conveyor drop to silos

The fabric filter will use bags with a maximum emission rate of 0.01 gr/dscf. The estimated stack flow rate and 0.01 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.01 grains/acf

PM = 2.85 lb/hr PM = 12 tons/yr PM10 = 2.85 lb/hr PM10 = 12 tons/yr

S18 Inactive Pile

The Inactive Pile will be approximately rectangular in shape. The approximate dimensions of the pile will be 2,080 feet by 1,035 feet at the base with a height of \$\frac{1}{2}\$ feet and a side slope of 2:1. To account for potential weekly disturbances, approximately 3.3% of the pile surface area is assumed to be affected by pile maintenance and is calculated as an active stockpile. The remaining 96.7%, the Inactive Portion, is assumed to be affected by wind erosion and is calculated as industrial wind erosion. Fugitive dust emissions will be controlled by dust suppression spray water plus surface crusting agents as necessary.

Emissions from Inactive Portion

Emissions are calculated using the EPA AP-42, Section 13.2.5 emission factor calculation for industrial wind erosion. PM emissions are assumed to be equal to PM30 emissions. Emissions from the pile are conservatively modeled using the fastest mile of wind recorded in the five years of Columbus meteorology data used for PSD modeling.

Emission factor : (g/m2/yr)

where

Based on the shape and the orientation to the prevailing wind direction guidance given in AP-42 Section 13.2.5, the inactive coal pile can be subdivided into three us/ur ratio subareas. These three subareas are used to calculate the equivalent friction velocity (u*).

1.12 Uncrusted Coal Pile From AP-42 Table 13.2.5-2

	Subarea #1	Subarea #2	Subarea #3
Surface Area, ft2	66,501	2,165,887	33,250
Subarea us/ur	0.2	0.6	0.9
Subarea us+	2.88	8.63	13
Subarea u*	0.29	0.86	1.30
Subarea u*t	1.12	1.12	1.12
Is u* < u*t?	Yes	Yes	No
Subarea Pi	0	0	6.16

u*t = Threshold friction velocity (m/s)

 PM Emission factor (g/m2/yr):
 6.16

 PM Emission factor (lb/ft2/hr):
 1.44E-07

 PM10 Emission factor (g/m2/yr):
 3.08

 PM10 Emission factor (lb/ft2/hr):
 7.21E-08

PM = 4.8E-03 lb/hr PM = 0.021 tons/yr PM10 = 2.4E-03 lb/hr PM10 = 0.010 tons/yr

Active Portion Pile Design Data

Surface area: 1.7 acres

Emissions from Active Portion

Emissions are calculated using the EPA AP-42, Section 11.9.1 emission factor calculation for an active storage pile (wind erosion and maintenance bulldozing). PM and PM10 emissions are computed as TSP <= 30 um. Use of TSP <= 30 um is a conservative estimate for PM10.

Emission factor : $\left(\frac{lb}{acre - hr} \right) = 0.72u$

where: u = average wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data

Emission factor: 7.06 lb/acre-hr

Control efficiency = 90% for water sprays and chemical suppressant

PM = 1.20 lb/hr PM = 5.25 tons/yr PM10 = 1.20 lb/hr PM10 = 5.25 tons/yr

Combined Emissions at Inactive Pile

PM = 1.20 lb/hr PM = 5.27 tons/yr PM10 = 1.20 lb/hr PM10 = 5.26 tons/yr

IV. ASH MANAGEMENT PARTICULATE SOURCES

Wastes produced by the boiler, scrubber, and fabric filter are grouped into two types, bottom ash and fly ash.

BOTTOM ASH

The term "bottom ash" is used to refer collectively to the boiler bottom ash and pyrite rejects. This waste stream is modeled as a separate waste stream for disposal in the On-Site Disposal Facility.

S19 Reserved

S20 Bottom Ash Transfer Point #1

Bottom ash from the boiler is collected by a submerged chain conveyor and dropped onto the bottom ash conveyor at Bottom Ash Transfer Point #1. The Facility may have a grinder for reducing the size of any large pieces of bottom ash, which will be placed between the submerged-chain conveyor and the bottom ash conveyor. A building will enclose the optional grinder and associated transfer points. Since AP-42 Section 11.24 lists emissions from wet grinding as negligible, the grinding operation and enclosed transfer points are not calculated. Instead, emissions are conservatively calculated for the single exposed Bottom Ash Transfer Point #1. The bottom ash will have a high surface moisture content thereby reducing emissions.

Bottom Ash Throughput Design Data

Maximum bottom ash transfer rate: 40 tons/hr

94,610 tons/yr Assumes full load operation for 8,760 hours per year

Emissions

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum expected throughput per year.

Emission factor : $\left(\frac{lb \ emissions}{ton \ ash} \right) = k * 0.0032 * \frac{ \left(\frac{U}{5} \right)^{1.3}}{ \left(\frac{M}{2} \right)^{1.4}}$

where: k = particulate multiplier = 1 for PMk = particulate multiplier = 0.35 for PM10

U = mean wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data M = material moisture content (%) = 20 average moisture content of bottom ash

PM Emission factor: 3.06E-04 lb/ton PM10 Emission factor: 1.07E-04 lb/ton

PM = 0.012 lb/hr PM = 0.014 tons/yr PM10 = 4.3E-03 lb/hr PM10 = 5.1E-03 tons/yr

S21 Reserved

S22 Bottom Ash Bunker

Bottom ash is dropped from the bottom ash conveyor into the Bottom Ash Bunker. The Bottom Ash Bunker will be partially enclosed. The bottom ash will have a high surface moisture content thereby reducing emissions.

Bottom Ash Throughput Design Data

Maximum bottom ash transfer rate: 40 tons/hr 94,610 tons/yr

Assumes full load operation for 8,760 hours per year

Emissions

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum expected throughput per year.

Emission factor:

$$\left(\frac{\text{lb emissions}}{\text{ton ash}}\right) = k * 0.0032 * \frac{\left(\frac{U}{5}\right)^{1.3}}{\left(\frac{M}{2}\right)^{1.4}}$$

where: $k = particulate multiplier = 1 for PM \\ k = particulate multiplier = 0.35 for PM10$

U = mean wind speed (mph) = 9.8

M = material moisture content (%) = 20 average moisture content of bottom ash

PM Emission factor: 3.06E-04 lb/ton PM10 Emission factor: 1.07E-04 lb/ton

PM = 0.012 lb/hr PM = 0.014 tons/yr PM10 = 4.3E-03 lb/hr PM10 = 5.1E-03 tons/yr

S23 Bottom Ash Transfer Point #2

The bottom ash will be loaded from the Bottom Ash Bunker into trucks for transport to the On-Site Disposal Facility. The bottom ash will have a high surface moisture content thereby reducing emissions.

Bottom Ash Throughput Design Data

Maximum bottom ash transfer rate: 150 tons/hr

94,610 tons/yr Assumes full load operation for 8,760 hours per year

Emissions

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum expected throughput per year.

Emission factor :

$$\left(\frac{\text{lb emissions}}{\text{ton ash}}\right) = k * 0.0032 * \frac{\left(\frac{U}{5}\right)^{1.3}}{\left(\frac{M}{2}\right)^{1.4}}$$

where: $k = particulate multiplier = 1 for PM \\ k = particulate multiplier = 0.35 for PM10$

U = mean wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data
M = material moisture content (%) = 20 average moisture content of bottom ash

PM Emission factor: 3.06E-04 lb/ton PM10 Emission factor: 1.07E-04 lb/ton

PM = 0.046 lb/hr PM = 0.014 tons/yr PM10 = 0.016 lb/hr PM10 = 5.1E-03 tons/yr

S24 Reserved

S25 Bottom Ash Transfer Point #3

The bottom ash will be dropped from the bottom ash trucks onto the Working Face of the On-Site Disposal Facility. The bottom ash will have a high surface moisture content thereby reducing fugitive emissions.

Bottom Ash Throughput Design Data

Maximum bottom ash transfer rate: 150 tons/hr

94,610 tons/yr Assumes full load operation for 8,760 hours per year

Emissions

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum expected throughput per year.

Emission factor :

$$\left(\frac{\text{lb emissions}}{\text{ton ash}}\right) = k * 0.0032 * \frac{\left(\frac{U}{5}\right)^{1.3}}{\left(\frac{M}{2}\right)^{1.4}}$$

where: k = particulate multiplier = 1 for PM

k = particulate multiplier = 0.35 for PM10 U = mean wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data

U = mean wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data
M = material moisture content (%) = 20 average moisture content of bottom ash

PM Emission factor: 3.06E-04 lb/ton PM10 Emission factor: 1.07E-04 lb/ton

PM = 0.046 lb/hr PM = 0.014 tons/yr PM10 = 0.016 lb/hr PM10 = 5.1E-03 tons/yr

FLY ASH MANAGEMENT PARTICULATE SOURCES

The term "fly ash" is used to refer collectively to the ash removed from the economizer and air heater and the fly ash and scrubber waste from the fabric filter. The fly ash may be transported off-site via rail and/or truck or may be disposed of on-site. If disposed of on-site, there will be more transfer points and more possibility of particulate matter emissions. To be conservative, emissions related to on-site disposal are calculated. For on-site disposal, the fly ash will be mixed with water prior to disposal. The mixing station may be located near the power island, or next to the on-site disposal facility. Location next to the power island will have higher emissions so for design purposes, it is located next to the power island.

S26 Fly Ash Silos

The fly ash will first be transported through pipes by pneumatic means from the boiler economizer and air heater hoppers and from the boile fabric filter to one or more Fly Ash Silos. The transfer of portions of the fly ash to multiple silos are modeled as one transfer of all fly ash to one silo. From the Fly Ash Silo(s), the fly ash will be pneumatically transferred to either the loading facility or a mixing chamber. Each silo vent will exhaust through a vent filter.

Filter Design Data

Stack Diameter 1.5 feet Stack Flow 6,972 dscfm

Emissions

The vent filter will use bags with a maximum emission rate of 0.02 gr/dscf. The estimated stack flow rate and 0.02 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.02 gr/dscf

PM = 1.20 lb/hr PM = 5.23 tons/yr PM10 = 1.20 lb/hr PM10 = 5.23 tons/yr

S27 Fly Ash Mixing Station

A pneumatic conveyor will transport the fly ash from the Fly Ash Silo(s) into a mixing station next to the boiler fabric filter. In the mixing station, the fly ash will be mixed with approximately 30% water to create a wet dough-like product. The mixing station will exhaust through a fabric filter

Filter Design Data

Stack Diameter 1.5 feet Stack Flow 6,640 dscfm

Emissions

The fabric filter will use bags with a maximum emission rate of 0.01 gr/dscf. The estimated stack flow rate and 0.01 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

PM Emission factor: 0.01 gr/dscf

PM = 0.57 lb/hr PM = 2.49 tons/yr PM10 = 0.57 lb/hr PM10 = 2.49 tons/yr

S28 Fly Ash Transfer Point #1 (Fly Ash Mixing Station to fly ash truck)

Fly ash will be dropped from the Fly Ash Mixing Station into fly ash trucks for transport to the On-Site Disposal Facility. The fly ash will be in a wet, dough-like form thereby minimizing fugitive emissions.

Fly Ash Throughput Design Data

Maximum hourly dry fly ash transfer rate: 200 tons/hr

Water added to fly ash: 30 % of wet mixture weight

Maximum hourly wet fly ash transfer rate: 286 tons/hr

Maximum annual dry fly ash transfer rate: 576,951 tons/yr Assumes full load operation for 8,760 hours per year

Water added to fly ash: 30 % of wet mixture weight

Maximum annual wet fly ash transfer rate: 824,216 tons/yr

Emissions

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum throughput per year.

Emission factor :

$$\left(\frac{\text{lb emissions}}{\text{ton ash}}\right) = k * 0.0032 * \frac{\left(\frac{U}{5}\right)^{1.3}}{\left(\frac{M}{2}\right)^{1.4}}$$

where: k = particulate multiplier = 1 for PM

k = particulate multiplier = 0.35 for PM10

U = mean wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data

M = material moisture content (%) = 30 average moisture content of wet fly ash mixture

PM Emission factor: 1.73E-04 lb/ton PM10 Emission factor: 6.06E-05 lb/ton

PM = 0.049 lb/hr PM = 0.071 tons/yr PM10 = 0.017 lb/hr PM10 = 0.025 tons/yr

S29 Reserved

S30 Fly Ash Transfer Point #2 (fly ash truck to On-Site Disposal Facility)

Fly ash will be transferred from the fly ash trucks to the On-Site Disposal Facility by drop operation. The fly ash will be in a wet, dough-like form thereby minimizing fugitive emissions.

Fly Ash Throughput Design Data

Maximum wet fly ash transfer rate: 286 tons/hr

824,216 tons/yr Assumes full load operation for 8,760 hours per year

Emissions

The EPA AP-42, Section 13.2.4 drop point emission factor calculation is used to estimate continuous drop operation PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate while annual emissions are calculated based on the maximum throughput per year.

Emission factor :
$$\left(\frac{lb \ emissions}{ton \ ash} \right) = k * 0.0032 * \frac{\left(\frac{U}{5} \right)^{1.3}}{\left(\frac{M}{2} \right)^{1.4}}$$

where: $k = particulate multiplier = 1 for PM \\ k = particulate multiplier = 0.35 for PM10$

U = mean wind speed (mph) = 9.8 average of 7 years of Ely SCRAM data

M = material moisture content (%) = 30 average moisture content of wet fly ash mixture

PM Emission factor: 1.73E-04 lb/ton PM10 Emission factor: 6.06E-05 lb/ton

PM = 0.049 lb/hr PM = 0.071 tons/yr PM10 = 0.017 lb/hr PM10 = 0.025 tons/yr

S31 Reserved

S32 On-Site Disposal Facility

The wet, dough-like fly ash mixture and bottom ash will be deposited into the On-Site Disposal Facility for permanent disposal. The fly ash mixture will solidify to a concrete-like substance within several hours thereby greatly reducing the potential for fugitive emissions. The On-Site Disposal Facility will consist of Earth Moving activities and Wind Erosion. Wind erosion will occur on the piles of cover material, top soil and the working cell of the disposal facility and is estimated at 10 acres. Once disposal in a cell has been completed, the area will be reclaimed to natural vegetation. Wet material, water sprays and surface crusting agents will be used to control fugitive emissions.

Emissions from Earth Moving

Emissions from earth moving are calculated using the EPA AP-42 Section 11.9 emission rate calculation for overburden bulldozing. PM emissions are assumed to be equal to TSP <= 30 emissions.

Emission factor:

(lb/hr) =
$$k * \frac{1 * s^{1.5}}{M^{1.4}}$$

where: k = particulate multiplier = 5.7 for PM k = particulate multiplier = 1 for PM15 s = material silt content (%) = 9.0 AP-42 Table 13.2.4-1 M = material moisture content (%) = 12.0 AP-42 Table 13.2.4-1 PM10 scaling factor from PM15 = 0.75 AP-42 Table 11.9

PM Emission factor: 4.75 lb/hr PM10 Emission factor: 0.62 lb/hr

Control efficiency: 75% for water sprays

PM = 1.19 lb/hr PM = 5.20 tons/yr PM10 = 0.16 lb/hr PM10 = 0.68 tons/yr

Emission from Wind Erosion

Emissions from wind erosion are calculated using the EPA AP-42 Section 11.9 emission factor for wind erosion of exposed areas. PM and PM10 emissions are computed as $TSP \le 30$ um. Use of $TSP \le 30$ um is a conservative estimate for PM10.

Area Design Data

Exposed Area: 10 acres

Emission factor: 0.38 ton / acre - yr

Control efficiency: 80.0% for water sprays and/or surface crusting agents

PM = 0.17 lb/hr PM = 0.76 tons/yr PM10 = 0.17 lb/hr PM10 = 0.76 tons/yr

Combined Emissions from On-Site Disposal Facility

PM = 1.36 lb/hr PM = 5.96 tons/yr PM10 = 0.33 lb/hr PM10 = 1.44 tons/yr

VI. CARBON HANDLING PARTICULATE SOURCES

S33 <u>Carbon Silo</u>

Halogenated Activated Carbon will be delivered to the Facility in pneumatic trucks. Trucks will blow the carbon into the Carbon Silo. From the Carbon Silo, the carbon will be pumped to the injection grid in the flue gas stream. The Carbon Silo will exhaust through a vent

Filter Design Data

Stack Diameter 1.0 feet Stack Flow 3,486 dscfm

Emissions

The vent filter will use bags with a maximum emission rate of 0.02 gr/dscf. The estimated stack flow rate and 0.02 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.02 gr/dscf

PM = 0.60 lb/hr PM = 2.62 tons/yr PM10 = 0.60 lb/hr PM10 = 2.62 tons/yr

VI. LIME HANDLING PARTICULATE SOURCES

S34 Reserved

S35 <u>Lime Railcar Unloading Station</u>

Lime will be delivered to the Facility in pneumatic trucks or railcars. If delivered by railcar, there will be more transfer points and more possibility of particulate matter emissions. To be conservative, railcar delivery is modeled. Railcars will be brought into a partially enclosed railcar unloading structure. The railcars will have doors on the bottom which will open to dump the lime, or the cars will be connected with a rotary coupling so they can be tipped to dump the lime. The lime will be dumped into an underground hopper. From the underground hopper the lime will be transferred to a short conveyor and then to the lime conveyor. The hopper, the short conveyor and two transfer points will all occur in an enclosed area under the Lime Railcar Unloading Station. Emissions from the enclosed area will vent through a fabric filter.

Filter Design Data

Stack Diameter 4.0 feet Stack Flow 42,200 dscfm

Emissions from Railcar Unloading

The fabric filter will use bags with a maximum emission rate of 0.01 gr/dscf. The estimated stack flow rate and 0.01 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.01 gr/dscf

PM = 3.62 lb/hr PM = 16 tons/yr PM10 = 3.62 lb/hr PM10 = 16 tons/yr

S36 Reserved

S37 <u>Lime Silo</u>

Lime will be transferred from the lime conveyor to the Lime Silo by drop operation. From the Lime Silo, the lime will be gravity fed to a mixing station. At the enclosed mixing station a slurry will be created. The Lime Silo will exhaust through a vent filter.

Filter Design Data

Stack Diameter 1.5 feet Stack Flow 6,972 dscfm

Emissions

The vent filter will use bags with a maximum emission rate of 0.02 gr/dscf. The estimated stack flow rate and 0.02 gr/dscf emission rate are used to estimate PM and PM10 emission rates. Hourly emissions are calculated based on the maximum hourly design rate. Annual emissions are calculated based on 8,760 hours of operation per year at the maximum hourly design rate.

Emission factor: 0.02 gr/dscf

PM = 1.20 lb/hr PM = 5.23 tons/yr PM10 = 1.20 lb/hr PM10 = 5.23 tons/yr

VII. ROADWAY PARTICULATE SOURCES

S38 <u>Unpaved Roadway Travel</u>

The Facility will have unpaved roads within the On-Site Disposal Facility. Ash transfer trucks will travel inside the On-Site Disposal Facility each day. One maintenance truck will travel the route approximately three times per day. Daily road travel is estimated according to the maximum expected trips per day. The unpaved roads will be covered with gravel and/or chemical suppressant. Speed will be controlled to minimize fugitive emissions.

Emissions

Emissions are calculated using the EPA AP-42, Section 13.2.2 emission factor calculation for unpaved roads. PM emissions are assumed to be equal to PM30 emissions. Emissions are conservatively estimated using maximum expected number of vehicle trips per day, 365 days per year

Emission factor: $lb/VMT = k * (s/12)^a (W/3)^b ((365 - P)/365)$

where:	k = particle size multiplier	=	4.9	per AP-42 Table 13.2.2-2 for PM30
	k = particle size multiplier	=	1.5	per AP-42 Table 13.2.2-2 for PM10
	s = surface silt content (%)	=	4.2	AP-42 Section 13.2.2 - Unpaved Roads Related Info
	W = mean vehicle weight (tons)	=	57.6	calculated below
	a = empirical constant	=	0.7	per AP-42 Table 13.2.2-2 for PM30
	a = empirical constant	=	0.9	per AP-42 Table 13.2.2-2 for PM10
	b = empirical constant	=	0.45	per AP-42 Table 13.2.2-2 for PM30
	b = empirical constant	=	0.45	per AP-42 Table 13.2.2-2 for PM10
	P = # of days with 0.01" precipitation	=	60	per AP-42 Figure 13.2.2-1
	VMT = vehicle miles traveled			

Summary of daily vehicle travel on unpaved roads:

vehicle type	VMT per trip	weight (tons)	trips per day	total VMT daily	weight x daily VMT
bottom ash trucks	1.5	57	85	127.5	7,268
fly ash trucks	1.5	59	148	222	13,098
maintenance vehicles	1.5	3	3	4.5	13.5
Totals				354	20,379
		mean vehic	de weight (to	nel –	57.6

PM Emission factor: 7.42 lb/VMT PM10 Emission factor: 1.84 lb/VMT

Control efficiency: 98% for gravel/chemical suppressant and speed reduction (Malcolm Pirnie Air Currents May 2000)

PM = 2.19 lb/hr PM = 10 tons/yr PM10 = 0.54 lb/hr PM10 = 2.38 tons/yr

S39 Paved Roadway Travel

All roads at the Facility other than on the interior of the On-Site Disposal Area will be paved. Daily road travel is estimated according to the maximum expected trips per day. Fugitive emissions will be controlled by water sprays and/or sweeping.

Emissions

Emissions are calculated using the EPA AP-42, Section 13.2.1 emission factor calculation for paved roads. PM emissions are assumed to be equal to PM30 emissions. Emissions are conservatively estimated using maximum expected number of vehicle trips per day, 365 days per

Emission factor

$$\left(\frac{\text{lb}}{\text{VMT}}\right) = \left(k\left(\frac{\text{sL}}{2}\right)^{.65}\left(\frac{\text{W}}{3}\right)^{1.5} - C\left(1-\frac{1.2P}{N}\right)^{.5}\right)$$

where:	k = particle size multiplier	=	0.082	per AP-42 Table 13.2-1.1 for PM30
	k = particle size multiplier	=	0.016	per AP-42 Table 13.2-1.1 for PM10
	sL = road surface silt loading (g/m ²)	=	0.015	AP-42 Page 13.2.1-10 for annual avg conditions
	W = avg vehicle weight (tons)	=	23.9	calculated below
	C = emission factor for 1980's data	=	0.00047	per AP-42 Table 13.2.1-2 for PM30
	C = emission factor for 1980's data	=	0.00047	per AP-42 Table 13.2.1-2 for PM10
	P = # of days with 0.01" precipitation	=	60	per AP-42 Figure 13.2.1-2
	N = # of days in calculation period	=	365	
	VMT = vehicle miles traveled			

Summary of daily vehicle travel on paved roads:

vehicle type	VMT per trip	weight (tons)	trips per day	total VMT daily	weight x daily VMT
Para tanal a	4.0	00	40	40	570
lime trucks	1.2	30	16	19	576
bottom ash trucks	0.6	57	85	52	2,938
fly ash trucks	0.4	59	148	59	3,493
carrbon trucks	1.2	15	2	2	36
ammonia trucks	1.3	19	15	20	371
employee/visitor cars	1.0	2	130	131	262
maintenance vehicles	4.0	3	10	40	120
miscellaneous delivery trucks	1.0	5	4	4	20
Totals				327	7,816
		avg vehicle	weight (ton:	s) =	23.9

PM Emission factor: 0.046 lb/VMT PM10 Emission factor: 8.8E-03 lb/VMT

PM = 0.63 lb/hr PM = 2.75 tons/yr PM10 = 0.12 lb/hr PM10 = 0.52 tons/yr

VIII. EMERGENCY DIESEL ENGINES

S40 through S43 Reserved

S44 <u>Emergency Diesel Engine Driven Generator</u>

An Emergency Diesel Engine Driven Generator will be installed at the Facility to provide electric power for safe plant shutdown and critical load operation in the event of loss of the electrical grid. Operation of the generator will be limited to weekly testing and emergency use.

Design Data

 Generator size
 1,500 KW

 Heat Rate
 15.5 MMBtu/Hr

 Annual Hours of Operation
 500 hr/yr

 Fuel Flow:
 112 gal/hr

 Annual Fuel:
 56,000 gal

Emissions

CO, NOx, PM, and PM10 emissions are based on the applicable NSPS Subpart IIII limits. VOC emissions are based on a vendor cutsheet for a Tier I compliant non-road diesel engine rated more than 560 kW. SO2 emissions are calculated assuming a fuel sulfur content of 15 ppm. H2SO4 emissions are calculated based on SO2 emissions and an assumed oxidatation rate of 2.5%.

CO g/kwh lb/hr ton/year	3.5 11.6 2.89
NOx g/kwh lb/hr ton/year	6.4 21 5.29
SO2 lb/MMBtu lb/hr ton/year	1.6E-03 0.024 6.1E-03
PM g/kwh lb/hr ton/year	0.20 0.66 0.17
PM10 g/kwh lb/hr ton/year	0.20 0.66 0.17
VOC lb/MMBtu lb/hr ton/year	0.10 1.55 0.39
H2SO4 lb/MMBtu lb/hr ton/year	6.0E-05 9.3E-04 2.3E-04

S45 <u>Emergency Diesel Engine Driven Firewater Pump</u>

The Facility will have a Diesel Engine Driven Firewater Pump for emergency situations. Operation of the firewater pump will be limited to weekly testing and emergency use.

Design Data

Firewater pump size: 450 hp
Heat Rate: 3.15 MMBtu/hr
Annual Hours of Operation: 150 hours
Fuel Flow: 23 gal/hr
Annual Fuel: 3,404 gal

Emissions

The EPA AP-42, Table 3.3-1 emission factors are used to estimate VOC emissions. NSPS Subpart IIII limits are used to estimate CO, NOx, PM, and PM10 emissions. SO2 emissions are calculated assuming a fuel sulfur content of 15 ppm. H2SO4 emissions are calculated based on SO2 emissions and an assumed oxidatation rate of 2.5%.

CO g/HP-hr lb/MMBtu lb/hr ton/year	2.6 0.82 2.57 0.19
NOx g/HP-hr lb/MMBtu lb/hr ton/year	3.0 0.94 2.97 0.22
SO2 lb/MMBtu lb/hr ton/year	1.6E-03 4.9E-03 3.7E-04
PM g/HP-hr lb/MMBtu lb/hr ton/year	0.15 0.05 0.15 0.011
PM10 g/HP-hr lb/MMBtu lb/hr ton/year	0.15 0.05 0.15 0.011
VOC lb/MMBtu lb/hr ton/year	0.35 1.10 0.083
H2SO4 lb/MMBtu lb/hr ton/year	6.0E-05 1.9E-04 1.4E-05

IX. STORAGE TANKS

Emissions from the storage tanks have been calculated in two ways, per EPA TANKS 4.09 for average conditions and with AP-42 for maximum hourly conditions.

ANNUAL EMISSION

Annual emissions are calculated using the EPA TANKS program version 4.09. Printouts of the results for each of the tanks follow these emissions calculations.

MAXIMUM HOURLY EMISSIONS

The Maximum Hourly Emissions are calculated using the EPA AP-42, Section 7.1 emission factor calculation for annual working losses.

Emission factor (Annual basis): $L_{\!\scriptscriptstyle W} = 0.0010 M_{\scriptscriptstyle \it V} P_{\scriptscriptstyle \it VA} Q K_{\scriptscriptstyle \it N} K_{\scriptscriptstyle \it P}$

where:

Lw= working loss, lb/yr

Mv= vapor molecular weight, lb/lb-mole

Pva= vapor pressure at daily average liquid surface temperature, psia

Q= annual net throughput, bbl year

Kn= turnover factor = 1 for turnovers less than or equal to 36 Kp= working loss product factor = 1 for gasoline and diesel fuel

Revised to estimate hourly emissions:

Emission factor (Hourly basis): $L_{\scriptscriptstyle W} = 0.0010 M_{\scriptscriptstyle V} P_{\scriptscriptstyle VA} Q$

where:

Lw= working loss, lb/hr

Mv= vapor molecular weight, lb/lb-mole Pva= vapor pressure at time of tank filling, psia

Q= hourly throughput, bbl

S46 330,000 Gallon Distillate Oil Storage Tank

The Facility will have a 330,000 gallon vertical fixed roof storage tank for low sulfur distillate fuel oil for use in the auxiliary boiler and the PC boilers during startup. The tank will be equipped with conservation vent valves. The fuel oil storage tank will be bermed to contain approximately 125% of the contents of the tank. The berm will be impervious to water and oil.

Tank System Design Data

Tank Shell Height = 40 ft Tank Diameter = 39 ft

Emissions

Annual breathing and working emissions for the tank were calculated per EPA TANKS 4.09 (see attached). The maximum hourly VOC emissions from the tank are calculated using AP-42 described above.

EPA Tanks Summary:

Annual VOC Emissions: 127 lb/yr

Tank Maximum Hourly Emissions:

Emission factor:

 $L_w = 0.0010 M_V P_{VA} Q$

where:

Lw= working loss, lb/hr

Mv=vapor molecular weight, lb/lb-mole=130lb/lb-molePva=vapor pressure at time of tank filling, psia=0.022psiaQ=hourly throughput, bbl=13bbl

Emission factor: 0.038 lb/hr

VOC = 0.038 lb/hr VOC = 0.063 tons/yr

S47 20,000 Gallon Diesel Fuel Storage Tank

The Facility will have a 20,000 gallon diesel fuel vertical fixed roof storage tank for use in plant vehicles. A fuel dispensing station will be located adjacent to the storage tank. The tank will be equipped with conservation vent valves.

Tank System Design Data

Tank Shell Height = 14 ft
Tank Diameter = 16 ft

Emissions

Annual breathing and working emissions for the tank were calculated per EPA TANKS 4.09 (see attached). The maximum hourly VOC emissions from the tank are calculated using AP-42 described above.

EPA Tanks Summary:

Annual VOC Emissions: 1.01 lb/yr

Tank Maximum Hourly Emissions:

Emission factor:

 $L_W = 0.0010 M_V P_{VA} Q$

where:

Lw= working loss, lb/hr

Mv=vapor molecular weight, lb/lb-mole=130lb/lb-molePva=vapor pressure at time of tank filling, psia=0.022psiaQ=hourly throughput, bbl=1.41bbl

Emission factor: 4.0E-03 lb/hr

VOC = 4.0E-03 lb/hr VOC = 5.1E-04 tons/yr

S48 2,000 Gallon Diesel Fuel Storage Tank

The Facility will have a 2,000 gallon horizontal storage tank for diesel fuel for use in the Emergency Diesel Fuel-Fired Generator. The tank will be equipped with conservation vent valves.

Tank System Design Data

Tank Shell Height = 12 ft Tank Diameter = 10 ft

Emissions

Annual breathing and working emissions for the tank were calculated per EPA TANKS 4.09 (see attached). The maximum hourly VOC emissions from the tank are calculated using AP-42 described above.

EPA Tanks Summary:

Annual VOC Emissions: 2.24 lb/yr

Tank Maximum Hourly Emissions:

Emission factor:

 $L_{W} = 0.0010 M_{V} P_{VA} Q$

where:

Lw= working loss, lb/hr

Mv=vapor molecular weight, lb/lb-mole=130lb/lb-molePva=vapor pressure at time of tank filling, psia=0.022psiaQ=hourly throughput, bbl=0.14bbl

Emission factor: 3.9E-04 lb/hr

VOC = 3.9E-04 lb/hr VOC = 1.1E-03 tons/yr

\$49 500 Gallon Diesel Fuel Storage Tank

The Facility will have a 500 gallon diesel fuel horizontal storage tank for use in the Emergency Diesel Fuel-Fired Firewater Pump. The tank will be equipped with conservation vent valves.

Tank System Design Data

Tank Shell Height = 6 ft
Tank Diameter = 9 ft

Emissions

Annual breathing and working emissions for the tank were calculated per EPA TANKS 4.09 (see attached). The maximum hourly VOC emissions from the tank are calculated using AP-42 described above.

EPA Tanks Summary:

Annual VOC Emissions: 0.38 lb/yr

Tank Maximum Hourly Emissions:

Emission factor:

 $L_W = 0.0010 M_V P_{VA} Q$

where:

Lw= working loss, lb/hr

Mv= vapor molecular weight, lb/lb-mole = 130 lb/lb-mole
Pva= vapor pressure at time of tank filling, psia = 0.022 psia
Q= hourly throughput, bbl = 6.8E-03 bbl

Emission factor: 1.9E-05 lb/hr

VOC = 1.9E-05 lb/hr VOC = 1.9E-04 tons/yr

S50 500 Gallon Unleaded Gasoline Storage Tank

The Facility will have a 500 gallon unleaded gasoline horizontal storage tank for use in plant vehicles. A fuel dispensing station will be located adjacent to the storage tank. The tank will be equipped with conservation vent valves.

Tank System Design Data

Tank Shell Height = 6 ft
Tank Diameter = 9 ft

Emissions

Annual breathing and working emissions for the tank were calculated per EPA TANKS 4.09 (see attached). The maximum hourly VOC emissions from the tank are calculated using AP-42 described above.

EPA Tanks Summary:

Annual VOC Emissions: 540 lb/yr

Tank Maximum Hourly Emissions:

Emission factor:

 $L_W = 0.0010 M_V P_{VA} Q$

where:

Lw= working loss, lb/hr

Mv=vapor molecular weight, lb/lb-mole=66lb/lb-molePva=vapor pressure at time of tank filling, psia=10.5psiaQ=hourly throughput, bbl=0.012bbl

Emission factor: 8.5E-03 lb/hr

VOC = 8.5E-03 lb/hr VOC = 0.27 tons/yr

S01, S02, and S03 Boiler HAP Emissions (each @ 530 MW for Entire Year)

 Megawatts (Net)
 530 MW

 Load Condition
 100%

 Megawatts (Gross)
 576

 Coal flow (lb/hr)
 636,158

 Coal Flow (tons/hr)
 318

 Heat Input (MMBtu/hr, HHV)
 5,216

HC 4.2E-0.2	Pollutant Code
HF	7647-01-0
Antimony (Sb)	7647-01-1
Antimony (Sb)	7664-39-3
Antimory (Sb)	7664-39-4
Beryllium (Be)	
Beryllium (Be)	
Cadmium (Cd) 3.3E-05 Ib/MMBtu 1.7E-01 99% A.G 1.7E-03 7.5E-03 Chromium (Cr) 1.4E-03 Ib/MMBtu 7.3E+00 99% A.G 7.3E-02 3.2E-01 Cobalt (Co) 5.0E-04 Ib/MMBtu 2.6E+00 99% A.G 2.6E-02 1.1E-01 Lead (Pb) 1.2E-03 Ib/MMBtu 6.3E+00 99% A.G 6.8E-01 3.0E+00 Manganese (Mn) 1.3E-02 Ib/MMBtu 6.3E+00 99% A.G 6.8E-01 3.0E+00 Mercury (Hg) 2.0E-05 Ib/MMBtu 6.3E+00 99% A.G 6.8E-01 3.0E+00 Mercury (Hg) 2.0E-05 Ib/MMBtu 7.3E+00 99% A.G 6.8E-01 3.0E+00 Mercury (Hg) 2.0E-04 Ib/MMBtu 7.3E+00 99% A.G 1.0E-02 3.2E-01 Selenium (Se) 2.0E-04 Ib/MMBtu 7.3E+00 99% A.G 1.0E-02 3.2E-01 Selenium (Se) 2.0E-04 Ib/MMBtu 7.3E+00 99% A.G 1.0E-02 4.6E-02 Formaldehyde 2.4E-04 Ib/non 7.6E-02 Formaldehyde 7.6E-04 2.4E-03 PAH - Acenaphthene 5.1E-07 Ib/non 8.0E-05 D 8.0E-05 D 8.0E-05 Soletone 7.6E-04 2.4E-03 PAH - Benzo(a)anthracene 2.5E-07 Ib/non 8.0E-05 D 8.0E-05 Soletone 7.6E-05 2.9E-04 PAH - Benzo(a)anthracene 8.0E-08 Ib/non 2.5E-05 D 2.5E-05 1.5E-04 PAH - Benzo(a)pyrene 3.8E-08 Ib/non 2.5E-05 D 3.5E-05 5.3E-05 PAH - Benzo(b)fluoranthene 1.1E-07 Ib/non 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b)fluoranthene 1.1E-07 Ib/non 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b)fluoranthene 1.1E-07 Ib/non 3.2E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b)fluoranthene 1.1E-07 Ib/non 3.2E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b)fluoranthene 1.1E-07 Ib/non 3.2E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b)fluoranthene 1.1E-07 Ib/non 3.2E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b)fluoranthene 1.1E-07 Ib/non 3.2E-05 D	
Chromium (Cr)	
Cobalt (Co) 5.0E-04 Ib/MMBtu 2.6E+00 99% A.G 2.6E-02 1.1E-01 Lead (Pb) 1.2E-03 Ib/MMBtu 6.3E+00 99% A.G 6.3E-02 2.7E-01 Manganese (Mn) 1.3E-02 Ib/MMBtu 6.3E+00 99% A.G 6.3E-01 3.0E+00 Mercury (Hg) 2.0E-05 Ib/mwhr 1.2E-02 B 1.2E-02 5.0E-02 Ib/mwhr 1.2E-02 B 1.2E-02 5.0E-02 S.0E-02 S.0E-03 S.0E-04 S.0E-04 S.0E-04 S.0E-04 S.0E-04 S.0E-04 S.0E-04 S.0E-05	
Lead (Pb)	
Manganese (Mn)	
Mercury (Hg)	
Nickel (Ni)	
Selenium (Se)	
Formaldehyde	
PAH - Biphenyl 1.7E-06 Ib/ton 5.4E-04 D 5.4E-04 2.4E-03 PAH - Acenaphthene 5.1E-07 Ib/ton 1.6E-04 D 1.6E-04 7.1E-04 PAH - Acenaphthylene 2.5E-07 Ib/ton 8.0E-05 D 8.0E-05 3.5E-04 PAH - Anthracene 2.1E-07 Ib/ton 6.7E-05 D 6.7E-05 2.9E-04 PAH - Benzo(a)anthracene 8.0E-08 Ib/ton 2.5E-05 D 2.5E-05 1.1E-04 PAH - Benzo(a)pyrene 3.8E-08 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b),fluoranthene 1.1E-07 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b),fluoranthene 1.1E-07 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b),fluoranthene 1.1E-07 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b),fluoranthene 1.1E-07 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b),fluoranthene 1.1E-07 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b),fluoranthene 1.1E-07 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(c),fl.ip)erylene 2.7E-08 Ib/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Fluoranthene 7.1E-07 Ib/ton 3.2E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 Ib/ton 2.3E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 Ib/ton 2.3E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 Ib/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 Ib/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Phenanthrene 2.7E-06 Ib/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - F-Wenne 3.3E-07 Ib/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - S-Methyl chrysene 2.2E-08 Ib/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 Ib/ton 4.8E-03 E 3.2E-02 4.0E-01 Benzylen 3.3E-05 Ib/ton 4.1E-01 E 4.1E-01 1.8E-00 Benzylen 3.3E-05 Ib/ton 4.1E-01 E 4.1E-01 1.8E-00 Benzylen 3.3E-05 Ib/ton 4.1E-01 E 4.1E-01 1.8E-00 Benzylen 3.3E-05 Ib/ton 4.2E-03 E 2.2E-03 9.8E-03 Chlorodentene 2.2E-05 Ib/ton 1.	50-00-0
PAH - Acenaphthylene	92-52-4
PAH - Acenaphthylene	83-32-9
PAH - Anthracene	208-96-8
PAH - Benzo(a)anthracene 8.0E-08 lb/ton 2.5E-05 D 2.5E-05 1.1E-04 PAH - Benzo(a)pyrene 3.8E-08 lb/ton 1.2E-05 D 1.2E-05 5.3E-05 PAH - Benzo(b)fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(k)fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(g,h)jperylene 2.7E-08 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(g,h)jperylene 2.7E-08 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Chrysene 1.0E-07 lb/ton 3.2E-05 D 3.2E-05 1.5E-04 PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluoranthene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 <td< td=""><td>120-12-7</td></td<>	120-12-7
PAH - Benzo(a)pyrene 3.8E-08 lb/ton 1.2E-05 D 1.2E-05 5.3E-05 PAH - Benzo(b),fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(k),fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(k),fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(g,h,i)perylene 2.7E-08 lb/ton 8.6E-06 D 8.6E-06 3.8E-05 PAH - Chrysene 1.0E-07 lb/ton 3.2E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Phenanthrene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH	56-55-3
PAH - Benzo(b), fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(b) fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(g, hi)perylene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(g, h.i)perylene 2.7E-08 lb/ton 8.6E-06 D 8.6E-06 3.8E-05 PAH - Chrysene 1.0E-07 lb/ton 3.2E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Phenanthrene 2.7E-06 lb/ton 4.6E-04 D 8.6E-04 3.8E-05 PAH -	50-33-8
PAH - Benzo(j)fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(j,hi)poranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(j,h,i)perylene 2.7E-08 lb/ton 8.6E-06 D 8.6E-06 3.8E-05 PAH - Chrysene 1.0E-07 lb/ton 3.2E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Pyrene 3.3E-07 lb/ton 4.6E-04 D 8.6E-04 3.8E-03 PAH - S-Methyl chrysene 2.2E-08 lb/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde	205-99-2
PAH - Benzo(k)fluoranthene 1.1E-07 lb/ton 3.5E-05 D 3.5E-05 1.5E-04 PAH - Benzo(g,h,i)perylene 2.7E-08 lb/ton 8.6E-06 D 8.6E-06 3.8E-05 PAH - Chrysene 1.0E-07 lb/ton 3.2E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Pyrene 2.7E-06 lb/ton 8.6E-04 D 8.6E-04 3.8E-03 PAH - S-Methyl chrysene 2.2E-08 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.0E-06 3.1E-05 Acrolein	205-82-3
PAH - Benzo(g,h,i)perylene 2.7E-08 lb/ton 8.6E-06 D 8.6E-06 3.8E-05 PAH - Chrysene 1.0E-07 lb/ton 3.2E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 D 1.3E-03 1.8E-05 D 1.9E-05 8.5E-05 D 1.9E-04 1.9E-03 1.9	207-08-9
PAH - Chrysene 1.0E-07 lb/ton 3.2E-05 D 3.2E-05 1.4E-04 PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Phenanthrene 2.7E-06 lb/ton 8.6E-04 D 8.6E-04 3.8E-03 PAH - Pyrene 3.3E-07 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - S-Methyl chrysene 2.2E-08 lb/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetaldehyde 5.7E-04 </td <td>191-24-2</td>	191-24-2
PAH - Fluoranthene 7.1E-07 lb/ton 2.3E-04 D 2.3E-04 9.9E-04 PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Phenanthrene 2.7E-06 lb/ton 8.6E-04 D 8.6E-04 3.8E-03 PAH - Pyrene 3.3E-07 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - S-Methyl chrysene 2.2E-08 lb/ton 1.0E-04 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 lb/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton	218-01-9
PAH - Fluorene 9.1E-07 lb/ton 2.9E-04 D 2.9E-04 1.3E-03 PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Phenanthrene 2.7E-06 lb/ton 8.6E-04 D 8.6E-04 3.8E-03 PAH - Pyrene 3.3E-07 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - S-Methyl chrysene 3.3E-07 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - S-Methyl chrysene 2.2E-08 lb/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 lb/ton 1.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton	206-44-0
PAH - Indeno(1,2,3-cd)pyrene 6.1E-08 lb/ton 1.9E-05 D 1.9E-05 8.5E-05 PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Phenanthrene 2.7E-06 lb/ton 8.6E-04 D 8.6E-04 3.8E-03 PAH - Pyrene 3.3E-07 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - S-Methyl chrysene 2.2E-08 lb/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 lb/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb	86-73-7
PAH - Naphthalene 1.3E-05 lb/ton 4.1E-03 D 4.1E-03 1.8E-02 PAH - Phenanthrene 2.7E-06 lb/ton 8.6E-04 D 8.6E-04 3.8E-03 PAH - Pyrene 3.3E-07 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - 5-Methyl chrysene 2.2E-08 lb/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 lb/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.2E-01 9.8E-01 Bromoform 3.9E-05 lb/ton <	193-39-5
PAH - Phenanthrene 2.7E-06 lb/ton 8.6E-04 D 8.6E-04 3.8E-03 PAH - Pyrene 3.3E-07 lb/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - 5-Methyl chrysene 2.2E-08 lb/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 lb/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.2E-01 9.8E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton <t< td=""><td>91-20-3</td></t<>	91-20-3
PAH - Pyrene 3.3E-07 Ib/ton 1.0E-04 D 1.0E-04 4.6E-04 PAH - 5-Methyl chrysene 2.2E-08 Ib/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 Ib/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 Ib/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 Ib/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 Ib/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 Ib/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 Ib/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 Ib/ton 1.2E-02 E 1.2E-02 5.4E-02 2-Chloroacetophenone 7.0E-06 Ib/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroform 5.9E-05 Ib/ton	85-01-8
PAH - 5-Methyl chrysene 2.2E-08 lb/ton 7.0E-06 D 7.0E-06 3.1E-05 Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 lb/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 7.0E-03 E 2.2E-03 9.8E-03 Chloroform 5.9E-05 lb/ton <t< td=""><td>129-00-0</td></t<>	129-00-0
Acetaldehyde 5.7E-04 lb/ton 1.8E-01 E 1.8E-01 7.9E-01 Acetophenone 1.5E-05 lb/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03	3697-24-3
Acetophenone 1.5E-05 lb/ton 4.8E-03 E 4.8E-03 2.1E-02 Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	75-07-0
Acrolein 2.9E-04 lb/ton 9.2E-02 E 9.2E-02 4.0E-01 Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	98-86-2
Benzene 1.3E-03 lb/ton 4.1E-01 E 4.1E-01 1.8E+00 Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	107-02-8
Benzyl chloride 7.0E-04 lb/ton 2.2E-01 E 2.2E-01 9.8E-01 Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	71-43-2
Bis(2-ethylhexyl)phthalate 7.3E-05 lb/ton 2.3E-02 E 2.3E-02 1.0E-01 Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	100-44-7
Bromoform 3.9E-05 lb/ton 1.2E-02 E 1.2E-02 5.4E-02 Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	117-81-7
Carbon disulfide 1.3E-04 lb/ton 4.1E-02 E 4.1E-02 1.8E-01 2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	75-25-2
2-Chloroacetophenone 7.0E-06 lb/ton 2.2E-03 E 2.2E-03 9.8E-03 Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	75-25-2
Chlorobenzene 2.2E-05 lb/ton 7.0E-03 E 7.0E-03 3.1E-02 Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	
Chloroform 5.9E-05 lb/ton 1.9E-02 E 1.9E-02 8.2E-02 Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	532-27-4
Cumene 5.3E-06 lb/ton 1.7E-03 E 1.7E-03 7.4E-03	108-90-7 67-66-3
	98-82-8
Cyanide 1.3E-05 Ib/MMBtu 6.8E-02 H 6.8E-02 3.0E-01	57-12-5
2,4-Dinitrotoluene 2.8E-07 Ib/ton 8.9E-05 E 8.9E-05 3.0E-01	121-14-2
2,4-Dimitrologere 2.8E-07 10/101 8.9E-05 E 8.9E-05 3.9E-04 Dimethyl sulfate 4.8E-05 1b/ton 1.5E-02 E 1.5E-02 6.7E-02	77-78-1
Ethyl benzene 9.4E-05 lb/ton 3.0E-02 E 3.0E-02 1.3E-01	100-41-4
Ethyl chloride 4.2E-05 lb/ton 1.3E-02 E 1.3E-02 5.9E-02	75-00-3
Ethylene dichloride 4.0E-05 lb/ton 1.3E-02 E 1.3E-02 5.6E-02	107-06-2

Ethylene dibromide	1.2E-06	lb/ton	3.8E-04	Е	3.8E-04	1.7E-03	106-93-4
Hexane	6.7E-05	lb/ton	2.1E-02	E	2.1E-02	9.3E-02	110-54-3
Isophorone	5.8E-04	lb/ton	1.8E-01	E	1.8E-01	8.1E-01	78-59-1
Methyl bromide	1.6E-04	lb/ton	5.1E-02	Е	5.1E-02	2.2E-01	74-95-3
Methyl chloride	5.3E-04	lb/ton	1.7E-01	E	1.7E-01	7.4E-01	74-87-3
Methyl ethyl ketone	3.9E-04	lb/ton	1.2E-01	E	1.2E-01	5.4E-01	78-93-3
Methyl hydrazine	1.7E-04	lb/ton	5.4E-02	E	5.4E-02	2.4E-01	60-34-4
Methyl methacrylate	2.0E-05	lb/ton	6.4E-03	E	6.4E-03	2.8E-02	80-62-6
Methyl tert butyl ether	3.5E-05	lb/ton	1.1E-02	E	1.1E-02	4.9E-02	1634-04-4
Methylene chloride	2.9E-04	lb/ton	9.2E-02	E	9.2E-02	4.0E-01	75-09-2
Phenol	1.6E-05	lb/ton	5.1E-03	E	5.1E-03	2.2E-02	108-95-2
Propionaldehyde	3.8E-04	lb/ton	1.2E-01	E	1.2E-01	5.3E-01	123-38-6
Tetrachloroethylene	4.3E-05	lb/ton	1.4E-02	E	1.4E-02	6.0E-02	127-18-4
Toluene	2.4E-04	lb/ton	7.6E-02	E	7.6E-02	3.3E-01	108-88-3
1,1,1-Trichloroethane	2.0E-05	lb/ton	6.4E-03	E	6.4E-03	2.8E-02	71-55-6
Styrene	2.5E-05	lb/ton	8.0E-03	E	8.0E-03	3.5E-02	100-42-5
Xylenes	3.7E-05	lb/ton	1.2E-02	E	1.2E-02	5.2E-02	1330-20-7
Vinyl acetate	7.6E-06	lb/ton	2.4E-03	E	2.4E-03	1.1E-02	108-05-4
2,3,7,8-TCDD	1.43E-11	lb/ton	4.5E-09	С	4.5E-09	2.0E-08	1746-01-6
	•		•	TOTAL	19	61	per boiler

A = Values based on avg plus one standard deviation from USGS Coalqual Database

Report to Congress evaluating HAP emissions from coal-fired boilers.

B = Proposed emission limit

C = Emission Factor Source: AP-42, Table 1.1-12, 5th edition (9/98)

D = Emission Factor Source: AP-42, Table 1.1-13, 5th edition (9/98)

E = Emission Factor Source: AP-42, Table 1.1-14, 5th edition (9/98)

F = A 95% control efficiency of the uncontrolled emission rate was assumed based on backup documentation for the 2000 EPA

G = A 99% control efficiency was assumed based on the 2000 EPA Report to Congress evaluating HAP emissions from coal-fired boilers.

H = Emission Factor Source: EEI EPRI Subcommittee Recommendation

S01, S02, and S03 Boiler HAP Emissions (Oil Firing)

 Heat Input (MMBtu/hr)
 782

 Fuel Heating Value (Btu/lb)
 19,200

 Fuel Density (Ib/gal)
 7.23

 Fuel Flow (Ib/hr)
 40,729

 Fuel Flow (gal/hr)
 5,633

Pollutant	Emission Factor	Units	Notes	Emission Rate (lb/hr)
Arsenic	4.0	lb/MMBtu	J	3.1E-03
Beryllium	3.0	lb/MMBtu	J	2.3E-03
Cadmium	3.0	lb/MMBtu	J	2.3E-03
Chromium	3.0	lb/MMBtu	J	2.3E-03
Copper	6.0	lb/MMBtu	J	4.7E-03
Lead	9.0	lb/MMBtu	J	7.0E-03
Mercury	3.0	lb/MMBtu	J	2.3E-03
Manganese	6.0	lb/MMBtu	J	4.7E-03
Nickel	3.0	lb/MMBtu	J	2.3E-03
Selenium Zinc	15.0 4.0	lb/MMBtu lb/MMBtu	J J	1.2E-02 3.1E-03
		lb/10 ³ gallon		
Benzene	2.14E-04	- J	<u> </u>	1.2E-03
Ethylbenzene	6.36E-05	lb/10 ³ gallon	<u> </u>	3.6E-04
Formaldehyde	3.30E-02	lb/10 ³ gallon	l	1.9E-01
Napthalene	1.13E-03	lb/10 ³ gallon	I	6.4E-03
1,1,1-Trichlorethane	2.36E-04	lb/10 ³ gallon	l	1.3E-03
Toluene	6.20E-03	lb/10 ³ gallon	1	3.5E-02
o-Xylene	1.09E-04	lb/10 ³ gallon	1	6.1E-04
Acenaphthene	2.11E-05	lb/10 ³ gallon	1	1.2E-04
Acenaphthylene	2.53E-07	lb/10 ³ gallon	1	1.4E-06
Anthracene	1.22E-06	lb/10 ³ gallon	I	6.9E-06
Benz(a)anthracene	4.01E-06	lb/10 ³ gallon	I	2.3E-05
Benzo(b,k)fluoranthene	1.48E-06	lb/10 ³ gallon	I	8.3E-06
Benzo(g,h,l)perylene	2.26E-06	lb/10 ³ gallon	I	1.3E-05
Chrysene	2.38E-06	lb/10 ³ gallon	I	1.3E-05
Dibenzo(a,h) anthracene	1.67E-06	lb/10 ³ gallon	I	9.4E-06
Fluoranthene	4.84E-06	lb/10 ³ gallon	I	2.7E-05
Fluorene	4.47E-06	lb/10 ³ gallon	I	2.5E-05
Indo(1,2,3-cd)pyrene	2.14E-06	lb/10 ³ gallon	I	1.2E-05
Phenanthrene	1.05E-05	lb/10 ³ gallon	I	5.9E-05
Pyrene	4.25E-06	lb/10 ³ gallon	ı	2.4E-05
OCDD	3.10E-09	lb/10 ³ gallon	ı	1.7E-08
			TOTAL	0.28

per boiler

I = Emission factor source: AP-42 Table 1.3-9 (9/98) for distillate oil

J = Emission factor source: AP-42 Table 1.3-10 (9/98) for distillate oil

S05 Auxiliary Boiler HAP Emissions

 Heat Input (MMBtu/hr)
 367

 Fuel Heating Value (Btu/lb)
 19,200

 Fuel Density (Ib/gal)
 7.23

 Fuel Flow (Ib/hr)
 19,115

 Fuel Flow (gal/hr)
 2,644

 Annual Operating Hours
 500

 Annual Fuel (gal)
 1,321,894

				Emissio	n Rates
Pollutant	Emission Factor	Units	Notes	lb/hr	tons/year
Arsenic	4.0	lb/MMBtu	J	1.5E-03	3.7E-04
Beryllium	3.0	lb/MMBtu	J	1.1E-03	2.8E-04
Cadmium	3.0	lb/MMBtu	J	1.1E-03	2.8E-04
Chromium	3.0	lb/MMBtu	J	1.1E-03	2.8E-04
Copper	6.0	lb/MMBtu	J	2.2E-03	5.5E-04
Lead	9.0	lb/MMBtu	J	3.3E-03	8.3E-04
Mercury	3.0	lb/MMBtu	J	1.1E-03	2.8E-04
Manganese	6.0	lb/MMBtu	J	2.2E-03	5.5E-04
Nickel	3.0	lb/MMBtu	J	1.1E-03	2.8E-04
Selenium	15.0	lb/MMBtu	J .	5.5E-03	1.4E-03
Zinc	4.0	lb/MMBtu	J	1.5E-03	3.7E-04
Benzene	2.14E-04	lb/103 gallon	<u> </u>	5.7E-04	1.4E-04
Ethylbenzene	6.36E-05	lb/10 ³ gallon	1	1.7E-04	4.2E-05
Formaldehyde	3.30E-02	lb/10 ³ gallon	1	8.7E-02	2.2E-02
Napthalene	1.13E-03	lb/10 ³ gallon	1	3.0E-03	7.5E-04
1,1,1-Trichlorethane	2.36E-04	lb/10 ³ gallon	1	6.2E-04	1.6E-04
Toluene	6.20E-03	lb/103 gallon	ı	1.6E-02	4.1E-03
o-Xylene	1.09E-04	lb/10 ³ gallon	1	2.9E-04	7.2E-05
Acenaphthene	2.11E-05	lb/10 ³ gallon	1	5.6E-05	1.4E-05
Acenaphthylene	2.53E-07	lb/10 ³ gallon	1	6.7E-07	1.7E-07
Anthracene	1.22E-06	lb/10 ³ gallon	1	3.2E-06	8.1E-07
Benz(a)anthracene	4.01E-06	lb/10 ³ gallon	1	1.1E-05	2.7E-06
Benzo(b,k)fluoranthene	1.48E-06	lb/10 ³ gallon	I	3.9E-06	9.8E-07
Benzo(g,h,I)perylene	2.26E-06	lb/10 ³ gallon	1	6.0E-06	1.5E-06
Chrysene	2.38E-06	lb/10 ³ gallon	1	6.3E-06	1.6E-06
Dibenzo(a,h) anthracene	1.67E-06	lb/10 ³ gallon	1	4.4E-06	1.1E-06
Fluoranthene	4.84E-06	lb/10 ³ gallon	1	1.3E-05	3.2E-06
Fluorene	4.47E-06	lb/10 ³ gallon	I	1.2E-05	3.0E-06
Indo(1,2,3-cd)pyrene	2.14E-06	lb/103 gallon	ı	5.7E-06	1.4E-06
Phenanthrene	1.05E-05	lb/10 ³ gallon	1	2.8E-05	6.9E-06
Pyrene	4.25E-06	lb/103 gallon	1	1.1E-05	2.8E-06
OCDD	3.10E-09	lb/10 ³ gallon	ı	8.2E-09	2.0E-09
			TOTAL	0.13	0.033

I = Emission factor source: AP-42 Table 1.3-9 (9/98) for distillate oil

J = Emission factor source: AP-42 Table 1.3-10 (9/98) for distillate oil

		(old Star	tup of 53	80 MW B	oiler, Co	al and #2	oil								
Startup Time (hours)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
Main Steam Flow (%MCR)	0	0	0	0	18	21	26	25	25	25	25	25	25	75	90	MAX
Coal Flow (pph)	0	0	0	9,940	19,880	39,760	79,520	159,040	159,040	159,040	159,040	159,040	159,040	477,119	572,542	636,158
Coal Flow (tons)	0	0	0	5	19,000	20	40	80	80	80	80	80	80	239	286	318
Distillate Fuel Flow (pph)	20,377	30,565	36,678	40,754	40,754	40,754	36,678	0	0	0	0	0	0	0	0	0
Distillate Fuel Flow (gallons)	2,818	4,228	5,073	5,637	5,637	5,637	5,073	0	0	0	0	0	0	0	0	0
Distillato Fasi Fish (gallons)	2,010	1,220	0,010	0,007	0,001	0,007	0,010		<u> </u>	- ŭ		<u> </u>	- ŭ	-	- ŭ	Ů
Coal Heat Input (MMBtu/hr)	0	0	0	82	163	326	652	1,304	1,304	1,304	1,304	1,304	1,304	3,912	4,695	5,216
Distillate Heat Input (MMBtu/hr)	391	587	704	782	782	782	704	0	0	0	0	0	0	0	0	0
Total Heat Input (MMBtu/hr)	391	587	704	864	945	1,109	1,356	1,304	1,304	1,304	1,304	1,304	1,304	3,912	4,695	5,216
Stack Exit Temp. (°F)	60	86	112	138	164	190	216	242	268	297	165	165	165	165	165	165
Stack Exit Flow (acfm)	124,546	186,819	224,183	275,039	273,624	320,800	392,509	377,412	377,412	377,412	377,412	377,412	377,412	1,132,237	1,358,684	1,509,649
Stack Exit Moisture (% by wt.)	4.5	4.5	4.5	4.5	5.0	6.0	6.5	7.0	8.0	8.7	8.7	8.7	8.7	9.0	9.0	9.51
OO (II- (II-AII-AID)	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
CO (lb/MMBtu)	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.15	0.15	0.15
NOx (lb/MMBtu) before SCR	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.25	0.25	0.25	0.25	0.25	0.25
NOx (lb/MMBtu) after SCR	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.25	0.25	0.25	0.25	0.23	0.25
TOX (ID/WINDLA) alter OOK	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.43	0.40	0.23	0.03	0.03	0.07	0.07	0.01
Max coal sulfur content (%)	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%	0.66%
Design coal sulfur content (%)	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%	0.46%
Max distillate sulfur content (%)	1.5E-05															
SO2 (lb/MMBtu) before scrubber	1.6E-03	1.6E-03	1.6E-03	0.11	0.19	0.33	0.54	1.12	1.12	1.12	1.12	1.12	1.12	1.12	1.12	1.12
SO2 (lb/MMBtu) after scrubber	1.6E-03	1.6E-03	1.6E-03	0.11	0.19	0.33	0.54	1.12	1.12	1.12	0.56	0.12	0.09	0.09	0.09	0.09
Coal ash content (%)	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%	5.31%
Distillate ash content (%)	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%	0.02%
PM total (lb/MMBtu) after baghouse	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038
PM10 total (lb/MMbtu) after baghouse	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038	0.038
PM filterable (lb/MMBtu) after baghouse PM10 filterable (lb/MMBtu) after baghouse	0.015 0.015															
PINTO IIILETADIE (ID/INIVIBIU) alter bagriouse	0.013	0.013	0.013	0.015	0.015	0.015	0.015	0.013	0.013	0.015	0.013	0.015	0.015	0.015	0.015	0.015
VOC (lb/MMBtu)	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	3.6E-03	3.6E-03	3.6E-03
VOC (ID/IVIIVIDIU)	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	3.0L-03	3.0L-03	3.0L-03
lead (lb/MMBtu)	0	0	0	1.7E-06	3.1E-06	5.3E-06	8.7E-06	1.8E-05								
fluoride (as HF) (lb/MMBtu)	0	0	0	1.8E-03	3.3E-03	5.7E-03	9.3E-03	1.9E-02	1.9E-02	1.9E-02	1.9E-02	9.7E-04	9.7E-04	9.7E-04	9.7E-04	9.7E-04
H2SO4 (lb/MMBtu) before scrubber	6.0E-05	6.0E-05	6.0E-05	4.1E-03	7.4E-03	0.013	0.021	0.043	0.043	0.043	0.043	0.043	0.043	0.043	0.043	0.043
H2SO4 (lb/MMBtu) after scrubber	6.0E-05	6.0E-05	6.0E-05	4.1E-03	7.4E-03	0.013	0.021	0.043	0.043	0.043	0.043	7.0E-03	4.8E-03	3.4E-03	3.4E-03	3.4E-03
					=	=										
Hg (lb/MMBtu)	0	0	0	3.5E-06	6.4E-06	1.1E-05	1.8E-05	3.7E-05	3.7E-05	3.7E-05	3.7E-05	2.5E-05	2.5E-05	2.5E-05	2.5E-05	2.5E-05
A	0	0	0	0	0	0	0	0	0	0	40	40	40	-	-	-
Ammonia (ppm)	0	0	0	0	0	0	0	0	0	0	10	10	10	5	5	5
HCI (lb/MMBtu)	0	0	0	3.9E-03	7.1E-03	1.2E-02	2.0E-02	4.1E-02	4.1E-02	4.1E-02	4.1E-02	2.1E-03	2.1E-03	2.1E-03	2.1E-03	2.1E-03
Tior (ID/MINIDIA)	U	U	U	J.JL-03	7.12-03	1.26-02	2.01-02	-7.1L-UZ	-T. IL-UZ	7.1L-UZ	-7.1L-UZ	Z.1L-03	2.16-03	2.16-03	Z.1L-03	Z. 1L-03
CO Emissions (lb/hr)	176.1	264.1	316.9	388.8	425.5	498.8	610.3	586.9	586.9	586.9	586.9	586.9	586.9	586.9	704.2	782.5
NOx Emissions (lb/hr)	176.1	264.1	316.9	388.8	425.5	498.8	610.3	586.9	586.9	586.9	326.0	117.4	117.4	273.9	328.6	365.2
SO2 Emissions (lb/hr)	0.6	0.9	1.1	92.5	183.8	366.4	731.4	1,460.6	1,460.6	1,460.6	730.3	156.5	117.4	352.1	422.5	469.5
PM Total Emissions (lb/hr)	14.9	22.3	26.8	32.8	35.9	42.1	51.5	49.6	49.6	49.6	49.6	49.6	49.6	148.7	178.4	198.2
PM10 Total Emissions (lb/hr)	14.9	22.3	26.8	32.8	35.9	42.1	51.5	49.6	49.6	49.6	49.6	49.6	49.6	148.7	178.4	198.2
PM Filterable Emissions (lb/hr)	5.9	8.8	10.6	13.0	14.2	16.6	20.3	19.6	19.6	19.6	19.6	19.6	19.6	58.7	70.4	78.2
PM10 Filterable Emissions (lb/hr)	5.9	8.8	10.6	13.0	14.2	16.6	20.3	19.6	19.6	19.6	19.6	19.6	19.6	58.7	70.4	78.2
VOC Emissions (lb/hr)	3.9	5.9	7.0	8.6	9.5	11.1	13.6	13.0	13.0	13.0	13.0	13.0	13.0	14.1	16.9	18.8
lead (lb/hr)	0	0	0	0.001	0.0029	0.006	0.012	0.023	0.023	0.023	0.023	0.023	0.023	0.070	0.085	0.094
HF (lb/hr)	0.00	0.00	0.00	1.58	3.15	6.30	12.60	25.21	25.21	25.21	25.21	1.26	1.26	3.78	4.54	5.04
H2SO4 (lb/hr)	0.023	0.035	0.042	3.54	7.03	14.02	27.99	55.91	55.91	55.91	55.91	9.13	6.22	13.30	15.96	17.74
Hg (lb/hr)	0	0	0	0	6.0E-03	0.012	0.024	0.048	0.048	0.048	0.048	0.033	0.033	0.10	0.12	0.13
ammonia (lb/hr)	0.00	0.00	0	0	0	12.27	0	0 53.47	0 53.47	52.47	45 53.47	45 2.74	45 2.74	23	23	23
HCI (lb/hr)	0.00	0.00	0.00	3.34	6.68	13.37	26.73	53.47	53.47	53.47	53.47	2.74	2.74	8.22	9.86	10.95
Allow for three hours for start-up and stabilization	of the dry	FGD eveto	m SCR or	nd ammonis	a feed evet	ems										
Thiow for three flours for start-up and stabilization	or the dry	i OD syste	ii, oor, ar	iu ammonii	a ieeu sysii	JIIIO.										
	1															
	1	1	1	1		L	L	L			L		1	1	1	1

TANKS 4.0 Report Page 1 of 6

TANKS 4.0.9d

Emissions Report - Detail Format Tank Indentification and Physical Characteristics

Identification

User Identification: S46

City: White Pine County

State: Nevada

Company: White Pine Energy Associates
Type of Tank: Vertical Fixed Roof Tank
Description: 330,000 Gallon #2 Oil Fuel Tank

Tank Dimensions

 Shell Height (ft):
 40.00

 Diameter (ft):
 39.00

 Liquid Height (ft):
 37.00

 Avg. Liquid Height (ft):
 18.50

 Volume (gallons):
 330,000.00

 Turnovers:
 15.00

 Net Throughput(gal/yr):
 4,950,000.00

Is Tank Heated (y/n): N

Paint Characteristics

Shell Color/Shade: White/White
Shell Condition Good
Roof Color/Shade: White/White
Roof Condition: Good

Roof Characteristics

Type: Dome

Height (ft) 0.00 Radius (ft) (Dome Roof) 39.00

Breather Vent Settings

Vacuum Settings (psig): -0.03 Pressure Settings (psig) 0.03

Meterological Data used in Emissions Calculations: Ely, Nevada (Avg Atmospheric Pressure = 11.73 psia)

TANKS 4.0 Report

TANKS 4.0.9d Emissions Report - Detail Format Liquid Contents of Storage Tank

S46 - Vertical Fixed Roof Tank White Pine County, Nevada

		Daily Liquid Surf. Temperature (deg F)			Liquid Bulk Temp Vapor Pressure (psia)			Vapor Mol.	Liquid Mass	Vapor Mass	Mol.	Basis for Vapor Pressure	
Mixture/Component	Month	Avg.	Min.	Max.	(deg F)	Avg.	Min.	Max.	Weight.	Fract.	Fract.	Weight	Calculations
Distillate fuel oil no. 2	Jan	36.86	30.44	43.28	44.59	0.0031	0.0031	0.0036	130.0000			188.00	Option 1: VP40 = .0031
Distillate fuel oil no. 2	Feb	39.42	33.04	45.79	44.59	0.0031	0.0031	0.0039	130.0000			188.00	Option 1: VP40 = .0031
Distillate fuel oil no. 2	Mar	42.11	35.41	48.81	44.59	0.0034	0.0031	0.0043	130.0000			188.00	Option 1: VP40 = .0031 VP50 = .0045
Distillate fuel oil no. 2	Apr	45.70	37.93	53.47	44.59	0.0039	0.0031	0.0052	130.0000			188.00	Option 1: VP40 = .0031 VP50 = .0045
Distillate fuel oil no. 2	May	50.02	41.46	58.57	44.59	0.0045	0.0033	0.0062	130.0000			188.00	Option 1: VP50 = .0045 VP60 = .0065
Distillate fuel oil no. 2	Jun	54.33	44.75	63.92	44.59	0.0054	0.0038	0.0075	130.0000			188.00	Option 1: VP50 = .0045 VP60 = .0065
Distillate fuel oil no. 2	Jul	57.80	48.01	67.59	44.59	0.0061	0.0042	0.0084	130.0000			188.00	Option 1: VP50 = .0045 VP60 = .0065
Distillate fuel oil no. 2	Aug	56.54	47.26	65.81	44.59	0.0058	0.0041	0.0080	130.0000			188.00	Option 1: VP50 = .0045 VP60 = .0065
Distillate fuel oil no. 2	Sep	52.10	43.17	61.02	44.59	0.0049	0.0035	0.0068	130.0000			188.00	Option 1: VP50 = .0045 VP60 = .0065
Distillate fuel oil no. 2	Oct	46.89	38.99	54.80	44.59	0.0041	0.0031	0.0055	130.0000			188.00	Option 1: VP40 = .0031 VP50 = .0045
Distillate fuel oil no. 2	Nov	41.15	34.67	47.62	44.59	0.0033	0.0031	0.0042	130.0000			188.00	Option 1: VP40 = .0031 VP50 = .0045
Distillate fuel oil no. 2	Dec	37.19	30.94	43.44	44.59	0.0031	0.0031	0.0036	130.0000			188.00	Option 1: VP40 = .0031

TANKS 4.0 Report

TANKS 4.0.9d Emissions Report - Detail Format Detail Calculations (AP-42)

S46 - Vertical Fixed Roof Tank White Pine County, Nevada

Month:	January	February	March	April	May	June	July	August	September	October	November	Decemb
Standing Losses (lb):	3.1450	2.7905	3.5387	4.5555	5.9290	7.5952	8.9363	8.1233	6.5088	4.9789	3.1778	3.04
Vapor Space Volume (cu ft):	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28.879.26
Vapor Density (lb/cu ft):	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.00
Vapor Space Expansion Factor:	0.0466	0.0460	0.0484	0.0566	0.0622	0.0698	0.0709	0.0671	0.0649	0.0575	0.0467	0.04
Vented Vapor Saturation Factor:	0.9960	0.9960	0.9957	0.9950	0.9943	0.9932	0.9923	0.9926	0.9937	0.9948	0.9958	0.99
ank Vapor Space Volume:												
Vapor Space Volume (cu ft):	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.2610	28,879.20
Tank Diameter (ft):	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0
Vapor Space Outage (ft):	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1
Tank Shell Height (ft):	40.0000	40.0000	40.0000	40.0000	40.0000	40.0000	40.0000	40.0000	40.0000	40.0000	40.0000	40.0
Average Liquid Height (ft):	18.5000	18.5000	18.5000	18.5000	18.5000	18.5000	18.5000	18.5000	18.5000	18.5000	18.5000	18.5
Roof Outage (ft):	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6
oof Outage (Dome Roof)												
Roof Outage (ft):	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6750	2.6
Dome Radius (ft):	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0
Shell Radius (ft):	19.5000	19.5000	19.5000	19.5000	19.5000	19.5000	19.5000	19.5000	19.5000	19.5000	19.5000	19.5
apor Density												
Vapor Density (lb/cu ft):	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0
Vapor Molecular Weight (lb/lb-mole):	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0031	0.0031	0.0034	0.0039	0.0045	0.0054	0.0061	0.0058	0.0049	0.0041	0.0033	0.0
Daily Avg. Liquid Surface Temp. (deg. R):	496.5315	499.0866	501.7812	505.3709	509.6850	514.0004	517.4667	516.2063	511.7655	506.5648	500.8183	496.8
Daily Average Ambient Temp. (deg. F):	24.5500	29.5000	34.5500	41.5000	50.5000	59.5000	67.5000	65.4500	56.2500	45.8500	34.1000	25.6
Ideal Gas Constant R												
(psia cuft / (lb-mol-deg R)):	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10
Liquid Bulk Temperature (deg. R):	504.2608	504.2608	504.2608	504.2608	504.2608	504.2608	504.2608	504.2608	504.2608	504.2608	504.2608	504.2
Tank Paint Solar Absorptance (Shell):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1
Tank Paint Solar Absorptance (Sneil):	0.1700	0.1700		0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1
	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1
Daily Total Solar Insulation	040.0040	4 004 4000	4 440 0040	4 000 04 40	0.400.0050	0.007.4007	0.007.4007	0.000.0007	4 700 4457	4 000 0070	070 7040	7400
Factor (Btu/sqft day):	810.6249	1,091.4088	1,443.2612	1,839.2142	2,102.8656	2,367.4687	2,327.4927	2,060.6687	1,768.1457	1,303.0279	873.7616	712.9
apor Space Expansion Factor												
Vapor Space Expansion Factor:	0.0466	0.0460	0.0484	0.0566	0.0622	0.0698	0.0709	0.0671	0.0649	0.0575	0.0467	0.0
Daily Vapor Temperature Range (deg. R):	25.6746	25.4991	26.8139	31.0747	34.2016	38.3412	39.1589	37.0968	35.7044	31.6184	25.9031	24.9
Daily Vapor Pressure Range (psia):	0.0005	0.0008	0.0012	0.0021	0.0029	0.0037	0.0042	0.0038	0.0032	0.0024	0.0011	0.0
Breather Vent Press. Setting Range(psia):	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0031	0.0031	0.0034	0.0039	0.0045	0.0054	0.0061	0.0058	0.0049	0.0041	0.0033	0.0
Vapor Pressure at Daily Minimum Liquid												
Surface Temperature (psia):	0.0031	0.0031	0.0031	0.0031	0.0033	0.0038	0.0042	0.0041	0.0035	0.0031	0.0031	0.0
Vapor Pressure at Daily Maximum Liquid	0.000.	0.0001	0.0001	0.0001	0.0000	0.0000	0.0012	0.0011	0.0000	0.0001	0.0001	0.0
Surface Temperature (psia):	0.0036	0.0039	0.0043	0.0052	0.0062	0.0075	0.0084	0.0080	0.0068	0.0055	0.0042	0.0
Daily Avg. Liquid Surface Temp. (deg R):	496.5315	499.0866	501.7812	505.3709	509.6850	514.0004	517.4667	516.2063	511.7655	506.5648	500.8183	496.8
Daily Min. Liquid Surface Temp. (deg R):	490.1129	492.7119	495.0777	497.6023	501.1346	504.4151	507.6770	506.9321	502.8394	498.6602	494.3426	490.6
Daily Max. Liquid Surface Temp. (deg R):	502.9502	505.4614	508.4846	513.1396	518.2354	523.5857	527.2564	525.4805	520.6916	514.4694	507.2941	503.1
Daily Ambient Temp. Range (deg. R):	30.3000	28.2000	27.7000	31.0000	33.6000	37.6000	39.0000	37.9000	37.9000	35.3000	30.2000	30.0
ented Vapor Saturation Factor												
Vented Vapor Saturation Factor:	0.9960	0.9960	0.9957	0.9950	0.9943	0.9932	0.9923	0.9926	0.9937	0.9948	0.9958	0.9
Vapor Pressure at Daily Average Liquid:												
Surface Temperature (psia):	0.0031	0.0031	0.0034	0.0039	0.0045	0.0054	0.0061	0.0058	0.0049	0.0041	0.0033	0.0
Vapor Space Outage (ft):	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.1750	24.
orking Losses (lb):	3.9580	3.9580	4.3354	4.9771	5.7494	6.8513	7.7365	7.4146	6.2806	5.1905	4.1633	3.9
Vapor Molecular Weight (lb/lb-mole):	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0
Vapor Pressure at Daily Average Liquid	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.0000	130.
	0.0001	0.0001	0.000 *	0.0000	0.0045	0.005	0.000*	0.0050	0.0040	0.0044	0.0000	_
Surface Temperature (psia):	0.0031	0.0031	0.0034	0.0039	0.0045	0.0054	0.0061	0.0058	0.0049	0.0041	0.0033	0.0

TANKS 4.0 Report

Net Throughput (gal/mo.):		412,500.0000						412,500.0000		412,500.0000	412,500.0000		
Annual Turnovers:	15.0000	15.0000	15.0000	15.0000	15.0000	15.0000	15.0000	15.0000	15.0000	15.0000	15.0000	15.0000	
Turnover Factor:	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	
Maximum Liquid Volume (gal):	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	330,000.0000	
Maximum Liquid Height (ft):	37.0000	37.0000	37.0000	37.0000	37.0000	37.0000	37.0000	37.0000	37.0000	37.0000	37.0000	37.0000	
Tank Diameter (ft):	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	39.0000	
Working Loss Product Factor:	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	
Total Losses (lb):	7.1030	6.7486	7.8741	9.5325	11.6784	14.4466	16.6728	15.5380	12.7894	10.1694	7.3411	7.0063	

TANKS 4.0 Report

TANKS 4.0.9d Emissions Report - Detail Format Individual Tank Emission Totals

Emissions Report for: January, February, March, April, May, June, July, August, September, October, November, December

S46 - Vertical Fixed Roof Tank White Pine County, Nevada

		Losses(lbs)	
Components	Working Loss	Breathing Loss	Total Emissions
Distillate fuel oil no. 2	64.57	62.33	126.90

TANKS 4.0 Report

Emissions Report - Detail Format TANKS 4.0

Tank Identification and Physical Characteristics

dentification

User Identification:

White Pine County

Nevada

City: State: Company: Type of Tank:

20,000 Gallon Diesel Fuel Tank White Pine Energy Associates Vertical Fixed Roof Tank

Tank Dimensions

Description:

Shell Height (ft): Diameter (ft):

14.00 16.00 14.00 20,000.00 2.00 40,000.00 Liquid Height (ft): Avg. Liquid Height (ft):

Net Throughput (gal/yr): Is Tank Heated (y/n):

Volume (gallons):

Turnovers:

z

Paint Characteristics

Shell Color/Shade: Shell Condition:

White/White Good White/White Good

Roof Color/Shade: Roof Condition:

Roof Characteristics Type:

Dome

Height (ft): Radius (ft) (Dome Roof):

Breather Vent Settings Vacuum Settings (psig): Pressure Settings (psig):

-0.03 0.03

TANKS 4.0 Emissions Report - Detail Format Liquid Contents of Storage Tank

						-							
	4	Daily Temper	Daily Liquid Surf. Temperatures (deg F)	2	Ciquid Bulk Temp.	Vapor Pi	Vapor Pressures (psia)	Ž	Vapor Mol.	Liquid Mass	Vapor Mass		Basis for Vapor Pressure
MixigrerComponent	MIGHTH	Yvg.	Mid.	Wex.	(aed L)	. Avg	Ivain.	Max.	weignt	-Fract.	Fract.	wegnt	Calculations
Distillate fuel oil no. 2	Jan	36.86	30.44	43.28	44.59	0.0031	0.0031	0.0037	130.0000			188.00	Option 1: VP40 = .0031
Distillate fuel oil no. 2	Feb	39.42	33.04	45.79	44,59	0.0031	0.0031	0.0040	130.0000			188.00	Option 1: VP40 = .0031
Distillate fuel oil no. 2	Mar	42.11	35,41	48.81	44,59	0.0035	0.0031	0.0044	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuet oil no. 2	Apr	45.70	37.93	53.47	44.59	0.0040	0.0031	0.0052	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Мау	50.02	41.46	58.57	44.59	0.0046	0.0034	0.0062	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Jun	54.33	44.75	63.92	44.59	0.0054	0,0039	0.0074	130,0000			188.00	Option 5: A=12.101, B=8907
Distiliate fuel oil no. 2	Jul	57.80	48.01	67.59	44.59	0.0060	0.0043	0.0083	130,0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Aug	56.54	47.26	65.81	44.59	0.0058	0.0042	0.0078	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Sep	52.10	43.17	61.02	44.59	0.0050	0.0037	2900.0	130,0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Oct	46.89	38,99	54.80	44.59	0.0042	0.0031	0.0055	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Nov	41.15	34.67	47.62	44.59	0.0034	0.0031	0.0043	130,0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Dec	37.19	30.94	43.44	44.59	0.b031	0.0031	0.0037	130.0000			188.00	Option 1: VP40 = .0031

December 0.0234 220.6549 0.0001 0.0452 0.9998	220.8549 16.0000 1.0974 14.0000 1.0974	1.0974 16.0000 8.0000	0.0001	0.0031 496.8623 25.6000	10.731 504.2608 0.1700 0.1700	712.9057	0.0452 24.9934 0.0006 0.0600	0.0031	0.0031	0.0037 496.8623 490.6139 503.1107 30.0000	0.9998	0.0031	0.0320
November 0.0254 220.6549 0.0001 0.0467 0.9998	220.6549 16.0000 1.0974 14.0000 1.0974	1.0974 16.0000 8.0000	0.0001	0.0034 500.8183 34.1000	10.731 504.2608 0.1700 0.1700	873.7616	0.0467 25.9031 0.0012 0.0600	0.0034	0.0031	0.0043 500.8183 494.3426 507.2941 30.2000	0.9998	0.0034	0.0354
October 0.0391 220.6549 0.0001 0.0575 0.9998	220,6549 16,0000 1,0974 14,0000 14,0000	1.0974 16.0000 8.0000	0.0001 130.0000	0.0042 506.5648 45.8500	10.731 504.2608 0.1700 0.1700	1,303.0279	0.0575 31.6184 0.0024 0.0600	0.0042	0.0031	0.0055 506.5648 498.6602 514.4694 35.3000	0.9998	0.0042	0.0429
September 0.0506 220.6549 0.0001 0.0649 0.9997	220,6549 16,0000 1,0974 14,0000 14,0000 1,0974	1.0974 16,0000 8.0000	0.0001	0.0050 511.7655 56.2500	10.731 504.2608 0.1700 0.1700	1,768.1457	0.0649 35.7044 0.0031 0.0600	0.0050	0.0037	0.0067 511.7655 502.8394 520.6916 37.9000	0.9997	0.0050	0.0513
August 0.0622 220.6549 0.0001 0.0671 0.9997	220.6549 16.0000 1.0974 14.0000 14.0000	1.0974 16.0000 8.0000	0.0001	0.0058 516.2063 65.4500	10.731 504.2608 0.1700 0.1700	2,060.6687	0.0671 37.0968 0.0036 0.0600	0.0058	0.0042	0.0078 516.2063 506.9321 525.4805 37.9000	0.9997	0.0058	0.0596
July 0.0684 220.6549 0.0001 0.0709 0.9996	220.6549 16.0000 1.0974 14.0000 14.0000	1.0974 16.0000 8.0000	0.0001 130.0000	0.0060 517.4667 67.5000	10.731 504.2608 0.1700	2,327.4927	0.0709 39.1589 0.0040 0.0600	0.0060	0.0043	0.0083 517.4667 507.5770 527.2564 39.0000	0.9996	0.0060 1.0974	0.0622 130.0000
June 0.0584 220.6549 0.0001 0.0698 0.9997	220.5549 16.0000 1.0974 14.0000 14.0000 1.0974	1.0974 16.0000 8.0000	0.0001	0.0054 514.0004 59.5000	10.731 504.2608 0.1700 0.1700	2,367.4687	0.0698 38.3412 0.0035 0.0600	0.0054	0.0039	0.0074 514.0004 504.4151 523.5857 37.6000	0.9997	0.0054 1.0974	0.0554 130.0000
May 0.0469 220.6549 0.0001 0.0622 0.9997	220.6549 16.0000 1.0974 14.0000 14.0000	1.0974 16.0000 8.0000	0.0001	0.0046 509.6850 50.5000	10.731 504.2608 0.1700 0.1700	2,102.8656	0.0622 34.2016 0.0027 0.0600	0.0046	0.0034	0,0062 509,6850 501,1346 518,2354 33,6000	0.9997	0.0046	0.0478
April 0.0358 220.6549 0.0001 0.0566 0.9998	220.6549 16.0000 1.0974 14.0000 14.0000 1.0974	1.0974 16.0000 8.0000	0.0001	0.0040 505.3709 41.5000	10,731 504,2608 0,1700 0,1700	1,839.2142	0.0566 31.0747 0.0021 0.0600	0.0040	0.0031	0.0052 505.3709 497.6023 513,1396 31.0000	0.9998	0.0040 1.0974	0.0412 130.0000
March 0.0281 220.6549 0.0001 0.0484 0.9998	220.6549 16.0000 1.0974 14.0000 14.0000 1.0974	1.0974 16.0000 8.0000	0.0001	0.0035 501.7812 34.5500	10.731 504.2608 0.1700 0.1700	1,443.2612	0.0484 26.8139 0.0013 0.0600	0.0035	0.0031	. 0.0044 501.7812 495.0777 508.4846 27.7000	0.9998	0.0035 1.0974	0.0363
February 0.0214 220.6549 0.0001 0.0461 0.9998	220.6549 16.0000 1.0974 14.0000 14.0000	1.0974 16.0000 8.0000	0.0001	0.0031 499.0866 29.5000	10.731 504.2608 0.1700 0.1700	1,091.4088	0.0461 25,4991 0.0609 0.0600	0.0031	0.0031	0.0040 499.0866 492.7119 505.4614 28.2000	0.9998	0.0031	0.0320
January 0.0241 220,6549 0.0001 0.0466 0.9998	220.6549 16.0000 1.0974 14.0000 14.0000	1.0974 16.0000 8.0000	0.0001	0.0031 496.5315 24.5500	10.731 504.2608 0.1700 0.1700	810.6249	0.0466 25.6746 0.0006 0.0600	0.0031	0.0031	0.0037 496.5315 490.1129 502.9502 30,3000	0.9998	0.0031 1.0974	0.0320
Month: Standing Losses (lb): Vapor Space Volume (cu ft): Vapor Space Expansion Factor: Vanted Vapor Saturation Factor:	Tank Vapor Space Volume Vapor Space Volume Vapor Space Volume (cu ft): Tank Diameter (ft): Vapor Space Outage (ft): Tank Shell Height (ft): Average Liquid Height (ft): Roof Outage (ft):	Roof Outage (Dome Roof) Roof Outage (ft): Dome Radius (ft): Sheil Radius (ft):	Vapor Density Vapor Density (Ib/cu ft): Vapor Molecular Weight ((Ib/b-mole): Vapor Molecular Weight ((Ib/b-mole): Vanco Bosense at Daile Accessed 1 solid	Veptor i ressure at Casa Average Liquid Surface Temperature (pisa): Daily Avez Liquid Surface Temp. (deg. R): Daily Average Ambient Temp. (deg. F): Ideal Gee Coorten	(psia cut / (lb-mol-deg R)): Liquid Bulk Temperature (deg. R): Tank Paint Solar Absorptance (Shell): Tank Paint Solar Absorptance (Roof): Paint Trial Solar Insulation	Factor (Blu/sqft day):	Vapor Space Expansion Factor Vapor Space Expansion Factor Daily Vapor Temporature Range (deg. R): Daily Vapor Pressure Range (psia): Breather Veri Press. Setting Range(psia): Vanna Pressure at Taily Avenae I in int	Surface Temperature (psia)	Surface Temperature (psia): Vanor Pressure at Daily Maximum Liquid	Surface Temperature (psia): Daliy Avg. Liquid Surface Temp. (deg R): Daliy Min. Liquid Surface Temp. (deg R): Daliy Max. Liquid Surface Temp. (deg R): Daliy Max. Liquid Surface Temp. (deg R): Daliy Ambient Temp. Range (deg. R):	Vented Vapor Saturation Factor Vented Vapor Saturation Factor: Vanor Pressure of Ingly Avance I legid	Surface Temperature (psia): Vapor Space Outage (ft):	Working Losses (Ib); Vapor Motecular Weight (Ib/Ib-mole); Vapor Pressure at Daily Average Liquid

TANKS 4.0 Emissions Report - Detail Format Individual Tank Emission Totals

		Losses(lbs)	
Components	Working Loss	Breathing Loss	Total Emissions
Distillate fuel oil no. 2	0.53	0.48	1.01

TANKS 4.0

Tank Identification and Physical Characteristics **Emissions Report - Detail Format**

dentification

User Identification:

City: State:

White Pine County

Nevada

Company: Type of Tank: Description:

White Pine Energy Associates Horizontal Tank 2,000 Galfon Diesel Fuel Tank

Tank Dimensions
Shell Length (ft):
Diameter (ft):
Volume (gallons):
Turnovers:

10.00 12.00 2,000.00 25.00 50,000.00

Net Throughput (gal/yr): Is Tank Heated (y/n): Is Tank Underground (y/n):

zz

Paint Characteristics Shell Color/Shade: Shell Condition:

White/White Good

Breather Vent Settings

-0.03 0.03

Vacuum Settings (psig): Pressure Settings (psig):

TANKS 4.0 Emissions Report - Detail Format Liquid Contents of Storage Tank

Mixture/Component	Month	Daily L Tempera Avg.	Daily Liquid Surf. Temperatures (deg F) rg. Min.	Max.	Liquid Bulk Temp. (deg F)	Vapor Pri Avg.	Vapor Pressures (psia) wg.	Max.	Vapor Mol. Weight	Liquid Mass Fract	Vapor Mass Fract	Mol. Weight	Basis for Vapor Pressure Calculations
Distillate fuel oil no. 2	Jan	36.86	30,44	43.28	44.59	0.0031	0.0031	0.0037	130.0000			188.00	Option 1: VP40 = .0031
Distillate fuel oil no. 2	Feb	39.42	33.04	45.79	44.59	0.0031	0.0031	0.0040	130.0000			188.00	Option 1: VP40 = .0031
Distillate fuel oil no. 2	Маг	42.11	35.41	48.81	44.59	0.0035	0.0031	0.0044	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Apr	45.70	37.93	53.47	44,59	0,0040	0.0031	0.0052	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Мау	50.02	41.46	58.57	44,59	0.0046	0.0034	0.0062	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Jun	54.33	44.75	63.92	44.59	0.0054	0.0039	0.0074	130.0000			188.00	Option 5; A=12.101, B=8907
Distillate fuel oil no. 2	JUI	57.80	48.01	62.59	44.59	0.0060	0.0043	0.0083	130.000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Aug	56.54	47.26	65.81	44.59	0.0058	0.0042	0.0078	130.0000			188.00	Option 5: A≂12.101, B≃8907
Distiliate fuel oil no. 2	Sep	52.10	43.17	61.02	44.59	0.0050	0.0037	0.0067	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Oct	46.89	38,99	54.80	44.59	0.0042	0.0031	0.0055	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Nov	41.15	34.67	47.62	44.59	0.0034	0.0031	0.0043	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Dec	37.19	30.94	43.44	44:59	0.0031	0.0031	0.0037	130.0000			188.00	Option 1: VP40 = .0031

ar December 9 0.0763 2 720.3652 11 0.0001 7 0.0452 9 0.9990	2 720.3652 0 12.0000 9 12.8639 0 6.0000 0 10.0000	0.0001	4 0.0031 3 496.8623 0 25.6000	11 10,731 18 504.2608 10 0.1700	712.9057	0.0452 11 24,9934 0.0006 0.0600	0.0031	0.0031	13 0.0037 33 496.8623 26 490.6139 14 503.1107 30.0000	0.9990	34 0.0031 30 6.0000	39 0.0400 30 130.0000	54 0.0031 57 4,166.6667 50 25,000 50 1.0000 50 12,0000 50 1.0000
November 0.0829 720.3652 0.0001 0.0467 0.9989	720.3652 12.0000 12.3639 6.0000 10.0000	0.0001	0.0034 500.8183 34.1000	1 10.731 3 504.2608 3 0.1700	9 873.7616	5 0.0467 4 25.9031 4 0.0012 0.0600	2 0.0034	1 0.0031	5 0.0043 8 500.8183 2 494.3426 4 507.2941 30.2000	7 0.9989	2 0.0034 0 6.0000	7 0.0439 0 130.0000	2 0.0034 7 4,166.6667 0 25.0000 0 12.0000 1.0000
October 0.1276 720.3652 0.0001 0.0575	720,3652 12,0000 12,3639 6,0000 10,0000	0.0001	0.0042 506.5648 45.8500	10.731 504.2608 0.1700	1,303.0279	0.0575 31.6184 0.0024 0.0600	0.0042	0.0031	0.0055 506.5648 498.6602 514.4694 35.3000	0.9987	0.0042	0.0537	0.0042 4,166,6667 25,0000 12,0000 12,0000
September 0.1649 720.3652 0.0001 0.0649 0.9884	720.3652 12.000 12.3639 6.0000 10.0000	0.0001 130.0000	0.0050 511.7655 56.2500	10.731 504.2608 0.1700	1,768.1457	0.0649 35.7044 0.0031 0.0600	0.0050	0.0037	0.0067 511.7655 502.8394 520.6916 37,9000	0.9984	0.0050	0.0642 130.0000	0.0050 4,166.6667 25.0000 12.0000 12.0000 1,0000
August 0.2027 720.3652 0.0001 0.0982	720.3652 12.0000 12.3639 6.0000	0.0001 130.0000	0.0058 516.2063 65,4500	10.731 504.2608 0.1700	2,060.6687	0.0671 37.0968 0.0036 0.0600	0.0058	0.0042	0.0078 516.2063 506.9321 525.4805 37.9000	0.9982	0.0058 6.0000	0.0745 130.0000	0.0058 4,166.667 25.0000 1.0000 12.0000 1.0000
July 0.2229 720.3652 0.0001 0.0709 0.3981	720,3652 12,0000 12,3639 6,0000 10,0000	0.0001 130.0000	0.0050 517.4667 67.5000	10.731 504.2608 0.1700	2,327.4927	0.0709 39.1589 0.0040 0.0600	0.0060	0.0043	0.0083 517.4667 507.6770 527.2564 39.0000	0.9981	0.0060	0.0777 130.0000	0.0060 4,166.6667 25,0000 12,0000 1,0000
June 0.1904 720.3652 0.0001 0.0598	720.3652 12.0000 12.3639 6.0000	0.0001	0.0054 514.0004 59.5000	10.731 504.2608 0.1700	2,367.4687	0.0698 38.3412 0.0035 0.0600	0.0054	0,0039	0.0074 514.0004 504.4151 523.5857 37.6000	0,9983	0.0054 6.0000	0.0692	0.0054 4,166.6867 25,0000 12,0000 1,0000
May 0.1528 720.3652 0.0001 0.0622 0.9985	720,3652 12.0000 12.3639 6.0000	0.0001	0.0046 509.6850 50.5000	10.731 504.2608 0.1700	2,102.8656	0.0622 34.2016 0.0027 0.0600	0.0046	0.0034	0.0062 509.6850 501.1346 518.2354 33.6000	0.9985	0.0046 6.0000	0.0598	0.0046 4,166.6567 25,0000 1,0000 12,0000 1,0000
April 0.1168 720.3652 0.0001 0.0566 0.5987	720,3652 12,0000 12,3639 6,0000	0.0001	0.0040 505.3709 41.5000	10.731 504.2608 0.1700	1,839.2142	0.0566 31.0747 0.0021 0.0600	0.0040	0.0031	0.0052 505.3709 497.6023 513.1396 31.0000	0,9987	0.0040	0.0515 130.0000	0.0040 4,166.8667 25.0000 1.0000 1.0000
March 0.0918 720.3652 0.0001 0.0484 0.9989	720.3652 12.0000 12.3639 6.0000 10.0000	0.0001 130.0000	0.0035 501.7812 34.5500	10.731 504.2608 0.1700	1,443.2612	0.0484 26.8139 0.0013 0.0600	0.0035	0.0031	0.0044 501.7812 495.0777 508.4846 27.7000	0.9989	0.0035	0.0454 130.0000	0.0035 4,166.6667 25.0000 1.0000 12.0000 1.0000
February 0.0698 720,3652 0.0001 0.0461 0.9990	720.3652 12.0000 12.3639 6.0000 10.0000	0.0001 130.0000	0.0031 499.0866 29.5000	10.731 504.2608 0.1700	1,091.4088	0.0461 25.4991 0.0009 0.0600	0.0031	0.0031	0.0040 499.0866 492.7119 505.4614 28.2000	0.9990	0.0031 6.0000	0.0400 130.0000	0.0031 4,186.6667 25.0000 1.0000 1.0000 1.0000
January 0.0787 720.3652 0.0001 0.0466 0.9990	720,3652 12,0000 12,3639 6,0000 10,0000	0.0001	0.0031 496.5315 24.5500	10.731 504.2608 0.1700	810.6249	0.0466 25.6746 0.0006 0.0600	0.0031	0.0031	0.0037 496.5315 490.1129 502.9502 30.3000	0.9990	0.0031	0.0400	0.0031 4,166,6667 25,0000 1,0000 12,0000 1,0000
Month: Slanding Losses (lb): Vapor Space Volume (cu ft): Vapor Density (lb/cu ft): Vapor Space Expension Factor: Vented Vapor Saturation Factor:	Tank Vapor Space Volume Vapor Space Volume (cu ft): Tank Dlameter (ft): Effective Diameter (ft): Vapor Space Outage (ft): Tank Shell Length (ft):	Vapor Density Vapor Density (Ib/cu ft); Vapor Molecular Weight (Ib/Ib-mole); Vapor Pressure at Daily Averace Liquid	Surface Temperature (psia): Daily Avg. Liquid Surface Temp. (deg. R): Daily Average Ambient Temp. (deg. F):	neal cas Constant R. (psia cuff (fb-mol-deg R)): Liquid Bulk Temperature (deg. R): Tank Pafit Solar Absorptance (Shell): Daliv Total Solar Institution	Factor (Btu/sqft day):	Vapor Space Expansion Factor Vapor Space Expansion Factor. Daily Vapor Temperature Range (deg. R): Daily Vapor Pressure Range (psia): Breather Vent Press. Setting Range(psia): Vanor Pressure at Daily Averane I initid	Surface Temperature (psia): Vanor Pressure at Dally Minimum Limited	Vanor Pressure at Daily Maximum I ionid	Surface Temperature (psia): Daily Avg. Liquid Surface Temp. (deg R): Daily Min. Liquid Surface Temp. (deg R): Daily Max. Liquid Surface Temp. (deg R): Daily Max. Liquid Surface Temp. (deg R): Verlack Varior Sahiratin Fardin	Vented Vapor Saturation Factor:	vapor riessure et cony vverage cupun Surface Temperature (psia): Vapor Space Outage (ft):	Working Losses (Ib): Vapor Molecular Weight (Ib/Ib-mole): Vanor Pressure at Daily Averana Innid	Surface Temperature (psia): Net Throughput (gal/mo.): Annual Turnovers: Turnover Factor: Tank Diameter (ft): Working Loss Product Factor:

	0.1163	
	0.1268	
-	0,1812	
	0.2291	
	0.2772	
	0.3006	
	0.2596	
	0.2125	
	0.1683	
	0,1372	
	0.1098	
	0.1187	
	Total Losses (lb):	

TANKS 4.0 Emissions Report - Detail Format Individual Tank Emission Totals

	Total Emissions	2.24
Losses(lbs)	Breathing Loss	1.58
and the second s	Working Loss	99:0
	Components	Distillate fuel oil no. 2

Tank Identification and Physical Characteristics **Emissions Report - Detail Format** TANKS 4.0

dentification

User Identification:

City: State:

Company: Type of Tank: Description:

Horizontal Tank 500 Gallon Diesel Fuel Tank

White Pine Energy Associates

White Pine County

Nevada

Fank Dimensions

Shell Length (ft):
Diameter (ft):
Volume (gallons):
Turnovers:
Net Throughput (gal/yr):
Is Tank Heated (y/n):
Is Tank Underground (y/n):

8.83 6.00 500.00 5.00 2,500.00

Paint Characteristics Shell Color/Shade:

zz

Shell Condition:

White/White

Good

Breather Vent Settings Vacuum Settings (psig): Pressure Settings (psig):

TANKS 4.0 Emissions Report - Detail Format Liquid Contents of Storage Tank

		Daily	Daily Liquid Surf.		Liquid Bulk				Vapor	Ljquid	Vapor		
Mixture/Component	Month	Тепре: Avg.	Temperatures (deg F) g. Min.	Мах.	Temp. (deg F)	Vapor P Avg.	Vapor Pressures (psia) Avg. Min.	Max.	Mol. Weight	Mass Fract.	Mass Fract.	Mol. Weight	Basis for Vapor Pressure Calculations
Distillate fuel oil no. 2	Jan	36.86	30.44	43.28	44.59	0.0031	0.0031	0.0037	130.0000			188.00	Option 1: VP40 = .0031
Distillate fuel oil no. 2	Feb	39.42	33.04	45.79	44.59	0.0031	0.0031	0.0040	130.0000			188.00	Option 1; VP40 = .0031
Distillate fuel oil no. 2	Mar	42.11	35.41	48.81	44.59	0.0035	0.0031	0.0044	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Apr	45.70	37.93	53.47	44.59	0.0040	0.0031	0.0052	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	May	50.05	41.46	58.57	44.59	0.0046	0.0034	0.0062	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Jun	54.33	44.75	63.92	44.59	0.0054	0.0039	0.0074	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Jul	57.80	48.01	62.79	44.59	0.0060	0.0043	0.0083	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Aug	56.54	47.26	65.81	44.59	0.0058	0.0042	0.0078	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Sep	52.10	43.17	61.02	44.59	0.0050	.0.0037	0.0067	130.0000			188.00	Option 5: A=12.101, B=8907
Distiliate fuel oil no. 2	Oct	46.89	38.99	54.80	44.59	0.0042	0.0031	0.0055	130.0000			188.00	Option 5: A=12,101, B≂8907
Distillate fuel oil no. 2	Nov	41.15	34.67	47.62	44.59	0.0034	0.0031	0.0043	130.0000			188.00	Option 5: A=12.101, B=8907
Distillate fuel oil no. 2	Dec	37.19	30.94	43.44	44.59	0.0031	0.0031	0.0037	130.0000			188.00	Option 1: VP40 = .0031

Month: January Standing Losses (tb): 0.0174 Vapor Space Volume (cu ft): 159.0206 Vapor Space Sxpansion Factor: 0.0466 Vapor Space Expansion Factor: 0.0466 Vented Vapor Saturation Factor: 0.0995	Tank Vapor Space Volume 159.0206 Vapor Space Volume (cu ft): 6.0000 Tank Diameter (ft): 8.2153 Vapor Space Outage (ft): 3.0000 Tank Shell Length (ft): 8.8300	Vapor Density Vapor Density (lb/cu ft): Vapor Molecular Weight (lb/b-mole): Vanor Presenre at Daily Averace I finite	Surface Temperature (psis): Daily Avez Liquid Surface Temp. (deg. R): 496.5315 Daily Average Ambient Temp. (deg. F): 24.5500	Ideal Gast Constant (10.731 (10.731 (10.731 Ideal Bulk Temperature (deg. R): 504.2608 (10.700 Polit Text Color Ideal Bulk Text Color Idea Bul	Dally Idal Sula Insulation Factor (Btu/sqft day):	Vapor Space Expansion Factor Vapor Space Expansion Factor O.0456 Daily Vapor Temperature Range (deg. R); 25.6746 Daily Vapor Peressure Range (psia); 0.0006 Vacor December 1 Press, Setting Range(psia); 0.0006	Value Pressure at Daily Average Liquid Sufface Temperature (psia) Vanco Percent (psia)	Vapor Pressure at Daily Millimum Englid Surface Temperature (psia) Vene Commence (psia)	Applor Pressure at Lawy Maximian Liquid Surface Temperature (psial) Daily Avg. Liquid Surface Temp. (deg R); 490.1128 Daily Max. Liquid Surface Temp. (deg R); 50.3500 Daily Max. Liquid Surface Temp. (deg R); 50.3500	Vented Vapor Saturation Factor Vented Vapor Saturation Factor	Vapor Fressure ar Dany Average Liquid Surface Temperature (psia): Vapor Space Outage (ft): 3.0000	Working Losses (lb): 0.0020 Vapor Molecular Weight (lb/lb-mole): 130.0000 Vapor Descript to August (land	Surface Temperature (psia): 0.0031 Net Throughput (gal/mo.): 208.3333 Annual Turnovers: 5.0000 Tank Diameter (ff): 6.0000 Working Loss Product Factor: 1.0000
February 0.0154 159.0206 0.0001 0.0461 0.9995	159,0206 6,0000 8,2153 3,0000 8,8300	0.0001	0.0031 499.0866 29.5000	10.731 504.2608 0.1700	1,091.4088	0.0461 25.4991 0.0009 0.0600	0.0031	0.0031	0.0040 499.0866 492.7119 505.4614 28.2000	0.9995	0.0031 3.0000	0.0020	0.0031 208.333 5.0000 1.0000 6.0000
March 0.0203 159.0206 0.0001 0.0484 0.9994	159,0206 6,0000 8,2153 3,0000 8,8300	0.0001	0.0035 501.7812 34.5500	10.731 504.2608 0.1700	1,443.2612	0.0484 26.8139 0.0013 0.0600	0.0035	0.0031	0.0044 501.7812 495.0777 508.4846 27.7000	0.9994	0.0035 3,0000	0.0023 130.0000	0.0035 208.3333 5.0000 1.0000 6.0000 1.0000
April 0.0258 159.0206 0.0001 0.0566 0.0994	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0040 505.3709 41.5000	10.731 504.2608 0.1700	1,839.2142	0.0566 31.0747 0.0021 0.0600	0.0040	0.0031	0.0052 505.3709 497.6023 513.1396 31.0000	0.9994	3.0000	0.0026	0.0040 208.3333 5.0000 1.0000 6.0000
May 0.0338 159.0206 0.0001 0.0622 0.9993	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0046 509.6850 50.5000	10.731 504.2608 0.1700	2,102.8656	0.0622 34.2016 0.0027 0.0600	0.0046	0.0034	0.0062 509.6850 501.1346 518.2354 33.6000	0.9993	3.0000	0.0030	0.0046 208.3333 5.0000 1.0000 1.0000
June 0.0421 159.0206 0.0001 0.0698 0.9991	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0054 514.0004 59.5000	10.731 504.2608 0.1700	2,367,4687	0.0698 38.3412 0.0035 0.0600	0.0054	0.0039	0.0074 514.0004 504.4151 523.5857 37.6000	0.9991	3.0000	0.0035	0.0054 208.333 5.0000 1.0000 6.0000 1.0000
July 0.0493 159.0206 0.0001 0.0709 0.9990	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0060 517.4667 67.5000	10.731 504.2608 0.1700	2,327.4927	0.0709 39.1589 0.0040 0.0600	0.0060	0.0043	0.0083 517.4667 507.6770 527.2564 39.0000	0.9990	0.0060	0.0039 130.0000	0.0080 208.3333 5.0000 1.0000 6.0000 1.0000
August 0.0448 159.0206 0.0001 0.0671	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0058 516.2063 65.4500	10.731 504.2608 0.1700	2,060,6687	0.0671 37.0968 0.0036 0.0600	0.0058	0.0042	0.0078 516.2063 506.9321 525.4805 37.9000	0.9991	0.0058	0.0037 130.0000	0.0058 208.3333 5.0000 1.0000 6.0000 1.0000
September 0.0364 159.0206 0.0001 0.0649 0.9992	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0050 511.7655 56.2500	10.731 504.2608 0.1700	1,768.1457	0.0649 35.7044 0.0031 0.0600	0.0050	0.0037	0.0067 511.7655 502.8394 520.6916 37.9000	0.9992	0.0050 3.0000	0.0032 130.0000	0.0050 208.3333 5.0000 1.0000 6.0000
October 0.0282 159.0206 0.0001 0.0575 0.9993	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0042 506.5648 45.8500	10.731 504.2608 0.1700	1,303.0279	0.0575 31.6184 0.0024 0.0600	0.0042	0.0031	0.0055 506.5648 498.6602 514.4694 35.3000	0.9993	3.0000	0.0027	0.0042 208.333 5.0000 1.0000 6.0000
November 0.0183 159.0206 0.0001 0.0467 0.9995	159.0206 6.0000 8.2153 3.0000 8.8300	0.0001	0.0034 .500.8183 34.1000	10.731 504.2608 0.1700	873.7616	0.0467 25.9031 0.0012 0.0600	0.0034	0.0031	0.0043 500.8183 494.3426 507.2941 30.2000	0.9995	0.0034 3.0000	0.0022	0.0034 208.333 5.0000 1.0000 6.0000 1.0000
December 0.0168 159.0206 0.0001 0.0452 0.9995	159,0206 6,0000 8,2153 3,0000 8,8300	0.0001	0.0031 496.8623 25.6000	10.731 504.2608 0.1700	712.9057	0.0452 24.9934 0.0006 0.0600	0.0031	0.0031	0.0037 496.8623 490.6139 503.1107 30.0000	0.9995	3.0000	0.0020	0.0031 208.3333 5.0000 1.0000 6.0000 1.0000

Page 3

0.0188	
0.0205	
0.0309	
0.0396	
0.0485	
0.0531	
0.0455	
0.0367	
0.0284	
0.0225	
0.0174	
0.0194	
Total Losses (lb):	

TANKS 4.0

Emissions Report - Detail Format Individual Tank Emission Totals

		Losses(lbs)	
Somponents	Working Loss	Breathing Loss	Total Emissions
Distillate fuel oil no. 2	0.03	0.35	0.38

Emissions Report - Detail Format TANKS 4.0

Tank Identification and Physical Characteristics

Identification User Identification:

City: State: Company: Type of Tank: Description:

Horizontal Tank 500 Gallon Unleaded Gasoline Tank

White Pine Energy Associates

White Pine County

Nevada

6.00 9.00 500.00 9.00 4,500.00

Tank Dimensions
Shell Length (ft):
Diameter (ft):
Volume (gallons):
Turnovers:

Net Throughput (gal/yr): Is Tank Heated (y/n): Is Tank Underground (y/n):

White/White Good

Paint Characteristics Shell Color/Shade: Shell Condition:

Vacuum Settings (psig): Pressure Settings (psig):

Breather Vent Settings

-0.03 0.03

TANKS 4.0 Emissions Report - Detail Format Liquid Contents of Storage Tank

		Daily L	Daily Liquid Surf.		Liquid Bulk				Vapor	Liquid	Vapor		
Mixture/Component	Month	Tempera Avg.	Temperatures (deg F) vg. Min.	Мах.	Temp. (deg F)	Vapor Pr Avg.	Vapor Pressures (psia) Avg. Min.	Мах.	Mol. Weight	Mass Fract.	Mass Fract	Mol. Weight	Basis for Vapor Pressure Calculations
Gasoline (RVP 10)	Jan	36.86	30.44	43.28	44.59	3.2423	2.8239	3.7094	66.0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	Feb	39.42	33.04	45.79	44.59	3.4222	2,9877	3.9064	66.0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	Маг	42.11	35.41	48.81	44.59	3.6205	3,1434	4.1546	66,0000			92.00	Option 4; RVP=10, ASTM Slope≍3
Gasoline (RVP 10)	Apr	45.70	37.93	53.47	44.59	3.8992	3,3167	4.5615	66.0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	May	50.02	41.46	58.57	44.59	4.2566	3,5721	5.0431	66.0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	unf	54.33	44.75	63.92	44.59	4.6401	3.8233	5.5917	66.0000			92.00	Option 4: RVP=10, ASTM Stope=3
Gasoline (RVP 10)	ĵnĵ	57.80	48.01	67.59	44,59	4.9679	4.0871	5.9950	66.0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	Aug	56.54	47.26	65,81	44.59	4.8467	4.0256	5.7971	66,0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	Sep	52.10	43.17	61.02	44.59	4.4382	3,7009	5.2893	66.0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	Oct	46.89	38.99	54.80	44.59	3.9956	3,3916	4.6835	99.0000			92.00	Option 4: RVP=10, ASTM Slope=3
Gasoline (RVP 10)	Nov	41.15	34.67	47.62	44.59	3.5486	3,0943	4.0554	0000799			92.00	Option 4: RVP=10, ASTM Stope=3
Gasoline (RVP 10)	Dec	37.19	30.94	43.44	44.59	3,2651	2.8549	3.7218	66.0000			92.00	Option 4: RVP=10, ASTM Slope=3

December 24.9371 243.1233 0.0404 0.1456 0.5622	243.1233 9.0000 8.2940 4.5000 6.0000	0.0404 66.0000 3.2651 496.8623 25.6000	10.731 504.2608 0.1700 712.9057	0.1456 24.9934 0.8668 0.0600	3.2651	3.7218 496.8623 490.6139 503.1107 30.0000	0.5622 3.2651 4.5000	1.9241 66.0000	3.2651 375.0000 9.0000 1.0000 9.0000 1.0000
November 27.8636 243.1233 0.0436 0.1619 0.5416	243.1233 9.0000 8.2940 4.5000 6.0000	0.0436 66.0000 3.5486 500.8183 34.1000	10.731 504.2608 0.1700 873.7616	0.1619 25.9031 0.9611 0.0600	3,5486	4.0554 500.8183 494.3426 507.2941 30.2000	0,5416 3,5486 4,5000	2.0911 66.0000	3.5486 375.0000 9.0000 1.0000 9.0000 1.0000
October 41.5018 243.1233 0.0485 0.2217 0.5120	243.1233 9.0000 8.2940 4.5000 6.0000	0.0485 66.0000 3.9956 506.5648 45.8500	10.731 504.2608 0.1700 1,303.0279	0.2217 31.6184 1.2919 0.0600	3.9956	4.6835 506.5648 498.6602 514.4694 35.3000	0.5120 3.9956 4.5000	2.3545 66.0000	3.9956 375.0000 9.0000 1.0000 9.0000
September 52.7940 243.1233 0.0533 0.2794 0.4858	243.1233 9.0000 8.2940 4.5000 6.0000	0.0533 66.0000 4.4382 511.7655 56.2500	10.731 504.2608 0.1700 1,768.1457	0.2794 35.7044 1.5884 0.0600	4.4382	5.2893 511.7655 502.8394 520.6916 37.9000	0.4858 4.4382 4.5000	2.6154 66.0000	4.4382 375,0000 9.0000 1.0000 9.0000 1.0000
August 64.5964 243.1233 0.0577 0.3205 0.4638	243.1233 9.0000 8.2940 4.5000 6.0000	0.0577 66.0000 4.8467 516.2063 65.4500	10.731 504.2608 0.1700 2,050.6687	0.3205 37.0968 1.7714 0.0600	4.8467	5.7971 516,2063 506,9321 525,4805 37,9000	0.4638 4.8467 4.5000	2.8561 66.0000	4.8467 375.0000 9.0000 1.0000 9.0000 1.0000
July 71.0709 243.1233 0.0590 0.3489 0.4577	243.1233 9.0000 8.2940 4.5000 6.0000	0.0590 66.0000 4.9679 517.4667 67.5000	10.731 504.2608 0.1700 2,327.4927	0.3489 39.1589 1.9079 0.0600	4.9679	5.9950 517.4667 507.6770 527.2564 39.0000	0.4577 4.9679 4.5000	2.9275 66.0000	4.9679 375.0000 9.0000 1.0000 9.0000
June 60.6552 243.1233 0.0555 0.3155 0.4747	243.1233 9.0000 8.2940 4.5000 6.0000	0.0555 66.0000 4.6401 514.0004 59.5000	10.731 504.2608 0.1700 2,367.4687	0.3155 38.3412 1.7684 0.0600	4,6401	5,5917 514,0004 504,4151 523,5857 37,6000	0.4747 4.6401 4.5000	2.7344	4.6401 375.0000 9.0000 1.0000 9.0000
May 49.1571 243.1233 0.0514 0.2559 0.4962	243.1233 9.0000 8.2940 4.5000 6.0000	0.0514 66.0000 4.2566 509.6850 50.5000	10.731 504.2608 0.1700 2,102.8656	0.2559 34.2016 1.4710 0.0600	4.2566	5.0431 509.6850 601.1346 518.2354 33.6000	0.4962 4.2566 4.5000	2.5084 66.0000	4.2566 375.0000 9.0000 1.0000 9.0000 1.0000
April 38.1591 243.1233 0.0475 0.2128 0.5181	243.1233 9.0000 8.2940 4.5000 6.0000	0.0475 66.0000 3.8992 505.3709 41.5000	10.731 504.2608 0.1700 1,839,2142	0.2128 31.0747 1.2448 0.0600	3.8992	4.5615 505.3709 497.6023 513.1396 31.0000	3.8992 4.5000	2.2977 66.0000	3.8992 375.0000 9.0000 1.0000 9.0000 1.0000
March 30.6430 243.1233 0.0444 0.1707 0.5366	243.1233 9.0000 8.2940 4.5000 6.0000	0.0444 65.0000 3.6205 501.7812 34.5500	10.731 504.2608 0.1700 1,443.2612	0.1707 26.8139 1.0112 0.0600	3.6205	4.1546 501.7812 495.0777 508.4846 27.7000	0.5366 3.6205 4.5000	2.1335 66.0000	3.6205 375.0000 9.0000 1.0000 9.0000 1.0000
February 24.4134 24.3.1233 0.0422 0.1544 0.5506	243.1233 9.0000 8.2940 4.5000 6.0000	0.0422 66.0000 3.4222 499.0866 29.5000	10.731 504.2608 0.1700 1,091,4088	0.1544 25.4991 0.9187 0.0600	3.4222	3.9064 499.0866 492.7119 505.4614 28.2000	0.5506 3.4222 4.5000	2.0166 66.0000	3,4222 375,0000 9,0000 1,0000 9,0000 1,0000
January 25,453 243,1233 0.0402 0.1490 0.5639	243.1233 9.0000 8.2940 4.5000 6.0000	0.0402 65.0000 3.2423 496.5315 24.5500	10.731 504.2608 0.1700 810.6249	0.1490 25.6746 0.8855 0.0600	3.2423	3,7094 496,5315 490,1129 502,9502 30,3000	0.5639 3.2423 4.5000	1.9106 66.0000	3.2423 375.0000 9.0000 1.0000 9.0000 1.0000
Month: Standing Losses (lb): Vapor Space Volume (cu ft): Vapor Density (lb/cu ft): Vapor Space Expansion Factor: Vented Vapor Saturation Factor:	Tank Vapor Space Volume Vapor Space Volume (cu ft): Tank Dlameter (ft): Effective Dlameter (ft): Vapor Space Outage (ft): Tank Shell Length (ft):	Vapor Density Vapor Density (lacu ft); Vapor Molecular Weight (la/lb-mole); Vapor Pressure at Daily Average Liquid Surface Temperature (psia); Daily Ave. Liquid Surface Temp. (deg. R); Daily Average Ambient Temp. (deg. F);	loear Joas Constant (psia cuft (lb-mol-deg R)); Liquid Bulk Temperature (deg. R); Tank Paint Solar Absorptance (Shell); Deily Total Solar Insulation Factor (Btu/sqft day);	Vapor Space Expansion Factor Vapor Space Expansion Factor: Daily Vapor Temperature Range (deg. R): Daily Vapor Pressure Range (psia): Breather Vent Press, Setting Range(psia): Vanor Pressure at Daily Avenare I in In	Surface Temperature (psia): Vapor Pressure at Daily Minimum Liquid Surface Temperature (psia):	vapor Pressure at Daily Maximum Liquid Surface Temperature (psia): Daily Avg. Liquid Surface Temp. (deg R): Daily Min. Liquid Surface Temp. (deg R): Daily Max. Liquid Surface Temp. (deg R): Daily Ambient Temp. Range (deg. R): Verhed Vannt Saturation Farther	Verited Vapor Saturation Factor: Vapor Pressure at Daily Average Liquid Surface Temperature (psia): Vapor Space Outage (ft):	Working Losses (lb): Vapor Molecular Weight (lb/lb-mole): Vapor Pressure at Daliy Average Liquid	Surface Temperature (psia): Net Throughput (gal/mo.): Annual Turnovers: Turnover Factor: Tank Diameter (ft): Working Loss Product Factor:

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26.8612	
29.9547	
43.8564	
55.4094	
67.5525	
73.9984	
63.3896	
51.8655	
40.4568	
32.7765	
26.4300	
27.3369	
Total Losses (lb):	

TANKS 4.0 Emissions Report - Detail Format Individual Tank Emission Totals

-		Losses(lbs)	
lients	Working Loss	Breathing Loss	l otal Emissions
Gasoline (RVP 10)	28.37	511.32	539.69